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DEPT. NAT. RES & ENV



PE710200

PEP 109
GHG 85A ROSEDALE
SEISMIC SURVEY



Hartogen Energy Limited



13 MAY 1986

PETROLEUM DIVISION

G 200

PEP 109

FINAL REPORT

GHG 85A ROSEDALE SEISMIC SURVEY

COMPILED BY S.R. GREAVES

HARTOGEN ENERGY LIMITED

MAY 1986

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INTRODUCTION

The GHG 85A Rosedale Seismic Survey was recorded in the onshore portion of the Gippsland Basin in Petroleum Exploration Permit 109 from 2 January 1985 to 21 February 1985.

Two hundred and seventy-two kilometres (272 km) of 85 fold, 512 channel Vibroseis data was recorded in the central and southern areas of PEP 109.

Data were processed by Geophysical Services International in Sydney, and data quality is very good.

The GHG 85A Rosedale Seismic Survey was programmed to provide control over the Seaspray and North Seaspray fault trends, and the regionally dominant Baragwanath Anticline.

The GHG 85A Rosedale Seismic Survey was operated by Hartogen Energy Limited on behalf of a consortium comprising:-

- Hartogen Energy Limited
- Cluff Oil (Pacific) Limited
- Plymouth Petroleum N.L.
- Poseidon Oil Pty Ltd

REGIONAL GEOLOGY AND STRATIGRAPHY

PEP 109 is located on the north west margin of the onshore portion of the Gippsland Basin. The Gippsland Basin is a wedge-shaped east to west trending basin. It is bounded to the north by the Victorian Ranges and to the south by the Bassian Rise, narrowing westward towards the Mornington Peninsula while it opens to the east towards the Tasman Sea. The Gippsland Basin has a high degree of north-south symmetry but in an east-west direction is asymmetrical with sediments thinning towards Mesozoic outcrops along its western margins and thickening eastwards in an offshore direction.

1. Structure

Structuring may be divided into two distinct periods: pre-Middle Eocene which consisted of extensional tectonics with normal faulting predominant. These features tended to trend north west to south east with throw down to the north east. The second phase of structuring is post-Middle Eocene with the main phase of structural activity being Middle Miocene to Recent and is caused by a compressional force acting from the south east. This has resulted in a series of north east to south west trending asymmetrical anticlines.

2. Stratigraphy

Basement consists of low grade metamorphics of Early to Middle Palaeozoic age intruded by Ordovician and Early Devonian granites. However, economic basement in petroleum exploration has normally been considered to be the Early Cretaceous Strzelecki Group. Strzelecki sediments were deposited on a rapidly but steadily subsiding fluvial plain. They consist predominantly of graywackes, subgraywackes, arkoses, chloritic mudstones, occasional coal, with local conglomerates, lavas and pyroclastic rocks. The sandstones are texturally mature but mineralogically immature and mostly impermeable. They are chloritic, feldspathic, volcanolithic, and of uniform fine to medium grain size with chloritic, kaolinitic, calcareous and sometimes pyritic cement. The shales have characteristic grey-green colour and are micaceous and slightly carbonaceous with silt laminae.

The Strzelecki Group is overlain by the Latrobe Group of Late Cretaceous to Late Eocene age. The Latrobe Group consists predominantly of fine to very coarse grained, poorly cemented quartzose sandstone with subordinate coal and grey or brown claystone and siltstone. The environment of deposition is interpreted to be fluvial, deltaic, lacustrine ranging to marginal marine. It thickens significantly to the east in the offshore area where it is estimated to reach up to 16,000 ft (5000 m) thick. The Latrobe Group contains prolific oil and gas accumulations in the offshore Gippsland Basin. The reservoir characteristics of the sandstones in the Latrobe are excellent with very high porosity and permeability sandstones. The hydrocarbon source for these accumulations is believed to be the lower part of the Latrobe, that is, Late Cretaceous and Early Paleocene. A regional seal to the Latrobe reservoir section is provided by the overlying Lakes Entrance Formation which consists of green, brown and grey calcareous claystone (marl) with thin limestone intercalations. The Gippsland Limestone consists of interbedded limestone and calcareous claystone or marl.

PREVIOUS EXPLORATION

Petroleum exploration in the area of PEP 109 commenced in the early 1960's and continued into the early 1970's, conducted mainly by Woodside and Arco. This exploration originally had as its main objective the Strzelecki Group with the emphasis moving to the Latrobe Group later in this period.

Early exploration provided only a sparse grid of poor-fair quality, mainly single fold seismic, and several wells. Upon reviewing all previous seismic, it is probable that none of the wells were located within closure at top Latrobe level and as such there is not a valid test of the Latrobe Group in the area.

Previous exploration has provided enough data to show that productive reverse fault trends offshore continue onshore with top Latrobe seals and excellent quality Latrobe Group reservoirs.

FIELD OPERATIONS

(A) Permitting, Line Clearing and Fencing

All permitting and property owner liaison was performed by K. Morrison of Hartogen Energy. In general few problems were encountered and good rapport was maintained between Hartogen's operations, property owners, local councils and the fire authorities.

Dozing was only required in areas of heavy growth and in some areas of the pine plantations. Use was made of the road network in PEP 109 to minimize access onto private property. The majority of clearing was accomplished by the use of a tractor-mounted slasher. Local contractors within the survey area were used for clearing, fencing and restoration work.

(B) Data Collection

The data collection contract was awarded to Geosystems Pty Ltd based in Perth.

Comparison recording between Litton LR5311 buggy-mounted vibrators and tractor-mounted Y600 vibrators was undertaken at the northern end of Line 85-07. The vibrators were used in the production array as well as singly over various frequency ranges.

The tractor-mounted vibrators demonstrated equivalent response at the Top Latrobe Group and Top Lakes Entrance reflectors (0.65 seconds and 0.35 seconds respectively), and increased resolution of shallow reflectors (0.2 to 0.3 seconds).

Hydraulic and electronic problems precluded the use of the tractor-mounted vibrators on a production basis.

A comprehensive report on the experimental and production recording is included as Appendix 1.

(C) Static Control

The long wavelength static profile was obtained by the drilling of upholes. The drilling was contracted to Fletcher Drilling Services Pty Ltd. Upholes were drilled at the beginning and end of all lines, at each intersection and at approximately 3 km intervals.

Poorly consolidated Quarternary sands and strata of brown coal caused occasional lost circulation and sticking problems. In all, 106 upholes were recorded in the prospect.

Uphole interpretation and static computations were performed by K.M. Frankcombe, consultant, and Geophysical Services Inc.

DATA PROCESSING

Data processing of the GHG 85A Rosedale Seismic Survey was performed by Geophysical Services International at their Sydney centre between March and June 1985.

A full programme of tests were produced and optimum parameters were selected prior to production processing of the data. A processing report by the contractor is included as Appendix 2, describing in detail the processes used.

INTERPRETATION

Mapping has been conducted at 1:25,000 scale on the near Top Lakes Entrance Formation and Near Top Latrobe Group reflectors. Ties were made to the Colliers Hill No. 1 well, which is the only well in the survey area to have a velocity survey. Other wells possessed a sonic log only and were integrated into the seismic where possible.

The Top Latrobe Group and Top Lakes Entrance Formation are the dominant reflectors on the data and can be readily followed over the area surveyed. The seismic reflector corresponding to the top Latrobe Group corresponds with a thick coal bed immediately beneath the Lakes Entrance Formation shales.

Carrs Creek No. 1 in the south east of PEP 109 encountered a medium grained, glauconitic sand between the top coal and Lakes Entrance shales. The edge of this sand can be seen on several of the GHG 85A lines and may form the basis of a stratigraphic trap across the Baragwanath Anticline. The sand is absent at North Seaspray No. 1.

The Strzelecki Group cannot be readily identified or mapped on the seismic. Most lines show a series of discontinuous, steeply dipping events beneath the known thickness of Latrobe Group sediments at the wells.

The major structural feature is the Baragwanath Anticline which exhibits a series of reverse faults on the northern limit. Plunging rapidly to the east, closure is not developed on the feature. Colliers Hill No. 1 was drilled on the axis and encountered the Latrobe Group sediments at 1800 ft. Both the Lakes Entrance and Top Latrobe Group subcrop beneath Quarternary sediments on the anticline in the north west corner of the survey area.

Regional dip to the south is seen between the Baragwanath Anticline and the North Seaspray feature. No evidence of structure is evident in the north eastern portion of the survey area.

The Seaspray and North Seaspray faults are two parallel reverse faults located in the southern portion of PEP 109. All major faulting revealed by the survey trends in an east-west direction. Movement on these faults appears to have occurred during the Eocene. The Seaspray and North Seaspray faults change direction to a north east-south west trend in the vicinity of Line 85A-16. Closure is developed on the upthrown side of both faults at the change of azimuth.

North Seaspray No. 1 tested the northern closure without encountering significant shows of hydrocarbons. The southern closure on the Seaspray fault exhibits smaller area and is not faulted at the Top Lakes Entrance Formation. This closure is now known as Burong.

Burong is presented as a four-way time closure at Top Latrobe Group level with approximately 450 acres (1.8 sq km) of fault-independent closure and 35 milliseconds of vertical time closure.

Of the wells in PEP 109 which possess a sonic log, a velocity inversion is apparent within the Lakes Entrance Formation (8300 ft/sec to 6600 ft/sec). Thickening of the Lakes Entrance Formation on the downthrown side of the North Seaspray and Seaspray faults leads to the possibility of distortion of the Top Latrobe Group time maps.

CONCLUSIONS AND RECOMMENDATIONS

The data produced from the GHG 85A Rosedale Seismic Survey was the first comprehensive grid of multifold data acquired in PEP 109. Resolution and continuity is superior to previous vintages of seismic data and has enabled detailed mapping of the main structural features in PEP 109.

Burong has been identified as a prospect and is considered to be mature for drilling.

Further seismic and/or gravity surveys should examine the northern part of PEP 109 and the possibility of a Top Latrobe Group stratigraphic play in the east. The swamp and lake conditions in the northern part of the Permit dictate the use of specialized equipment for any future work.

S.R. Greaves

May 1986

APPENDIX 1

ROSEDALE SEISMIC SURVEY 1985

GIPPSLAND BASIN

FINAL REPORT - OPERATIONS

BY

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OF

PARTY 204

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A wholly owned subsidiary of Geophysical
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for

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1. INTRODUCTION

The Rosedale Seismic Survey was carried out by Party 204 of Geo Systems of Carlisle, Western Australia for Hartogen Energy Ltd., Sydney, N.S.W. 272.55 kilometres approximately of 85 fold, 512-channel reflection profiling was recorded between 3rd January, 1985 and 21st February, 1985.

This report covers various field operations relating to line clearing, experimental survey, chaining and survey crews, recording and processing.

1.1 GEOGRAPHIC AREA

The Rosedale Prospect was located in the Gippsland Basin, Victoria, in Permit PEP.94 which is operated by Hartogen Energy Ltd. of Sydney, N.S.W. The approximate area is marked on the 1:100,000 Map Sheet (See Plate "A").

1.2 WEATHER

The weather conditions were generally fine and warm. The temperature ranged between 15° and 32°. There were a few overcast days and rain fell occasionally.

1.3 TERRAIN

The Survey Area was situated approximately 20 kms South-East of Sale. Large areas of the prospect were flat open grazing country (sheep, cattle and wheat production). Some parts were covered with pine tree plantations. The area around Boundary Creek in the North-West was hilly in parts, and areas along the coast line were swampy. The soils in the area were predominantly sandy.

1.4 LOGISTICS

The crew was accommodated at the Ambassador Motor Hotel in Sale. Supplies were obtained in Sale and Perth.

1.4 LOGISTICS (Cont'd)

Access to the area was along seismic lines and good existing roads.

Daily communications were by telephone to Geo Systems' Perth office.

1.5 RECORDING

Experimental parameter testing was conducted on the 2nd January, 1985 on Line 85-07. Production recording commenced on the 3rd January, 1985. A total of 272.55 kms of multifold seismic data was recorded. The programme consisted of 21 lines, which were oriented as follows:

- 1 Bearing North to South
- 7 Bearing North-West to South-East
- 2 Bearing North-East to South-West
- 11 Bearing approx. North-South

There were 368.75 recording hours, 33.00 hours daily testing, 49.00 hours travel time and 41.75 hours equipment downtime and/or lost recording time, for a total of 492.50 hours. The average rate of production was 0.553 kms per hour or 5.53 kms for a 10 hour production day. This rate includes travel, daily testing, daily downtime and line change.

2. SURVEYING

2.1 SUMMARY

The Rosedale Seismic Survey was undertaken on the 28th December, 1984 for Hartogen Energy. The total length of the prospect was 273.49 kms surveyed on seismic lines and approx. 60 kms was surveyed for traverse to and from Trig Stations and old PM's. The survey area was situated approx. 20 kms at centre point South-East of Sale, Victoria.

Datum take off was Colliers Hill Trig Station. Ties were made to other trigonometrical stations within the prospect.

Surveying was by Reciprocal Angle Levelling to ensure accurate vertical control. Sun shots were used for horizontal control. All closures within our work (Vert. = $0.05 \sqrt{\text{kms}}$, Horizontal = $0.25 \sqrt{\text{kms}}$) are in tolerance. (See Loop Closure Map). Permanent Markers were placed at start, finish, at bends, intersections and approx. 5 km intervals along lines. These consist of an Iron Picket driven to ground level with a witness post, both set in concrete, with aluminium tags attached. All stations occupied (turning points) were marked by a 30 centimetre peg placed at ground level. Stations were marked and chained at 30 metre intervals by a 50 centimetre peg and intermediate stns of 10 metres by flagging.

Survey Equipment Used:

- 1 Wild T16 Instrument
- 1 Wild T1A Instrument
- 2 Sokkisha Red 1A EDM's
- 2 HP 41CX Calculators
- 1 Printer
- Various tripods and prisms
- 2 Toyota Pick Up Trucks

2.2 LINE CLEARING

Line cutting was by a local contractor from Sale, hired by Hartogen Energy Ltd. Equipment used:

1 D6 Cat

1 D3 Cat

55.0 kms of seismic lines were bulldozed, mainly through pine forest plantations (See Appendix "B" for details).

3. PERMITTING AND PUBLIC RELATIONS

All permitting had been completed by a representative of Hartogen Energy Ltd. prior to commencement of the seismic survey.

4. RECORDING

4.1 EXPERIMENTAL

Experimental testing of recording parameters was carried out on VP #515, line 85-07 on 2nd January, 1985 using the following line parameters:

- 512 channels live
- 10 m geophone group interval
- 6 geophones per group at 1.67 m intervals
- split spread 2560 - 0 - 2560 m

The following are the tests undertaken:

Test	Vibe Type	Nº of Vibes	Frequency Range	Nº of Comps	Sweep Length	Move-Up	% Drive
1	Buggy	3	8-90	6	8 sec	None	30
2	"	"	10-90	"	"	"	"
3	"	"	12-90	"	"	"	"
4	"	"	14-90	"	"	"	"
5	"	"	16-90	"	"	"	"
6	"	"	18-90	"	"	"	"
7	"	"	20-90	"	"	"	"
8	"	"	8-90	"	"	4 m	"
9	"	"	10-90	"	"	"	"
10	"	"	12-90	"	"	"	"
11	"	"	12-96	"	"	"	"
12	"	"	12-100	"	"	"	"
13	"	"	12-110	"	"	"	"
14	"	"	8-64, 8-76, 10-80, 10-90, 12-96, 12-96	"	"	"	"
15	Tractor	1 (Nº 1)	12-96	1	"	None	"

4.1 EXPERIMENTAL (Cont'd)

Test	Vibe Type	N° of Vibes	Frequency Range	N° of Comps	Sweep Length	Move-Up	% Drive
16	Tractor	1 (N° 2)	12-96	1	8 sec	None	30
17	"	2 (N° 1&2)	"	6	"	4 m	"
18	Buggy	1 (N° 4)	"	1	"	None	"
19	"	1 (N° 2)	"	"	"	"	"
20	"	2 (N° 2&4)	"	6	"	4 m	"
21	"	1 (N° 1)	"	1	"	None	"
22	"	3	"	6	"	4 m	"
23	Tractor	1 (N° 4)	"	1	"	None	"
24	"	3	"	6	"	4 m	"

SUMMARY

Tests 1-7 were run to try and ascertain the optimum low end of the frequency range by keeping the top end constant (at 90 Hz). Test 3, 12-90 Hz, was considered the best in this series.

Tests 8-10 tested the use of move-ups as compared to the stationary sources used initially. These were superior in that the use of 4 m move-ups helped to reduce the amount of destructive noise generated. The three vibrators were 10 m apart from each other (pad to pad distance).

Keeping the low end constant at 12 Hz, Tests 11-13 tested increased the high end of the frequency range to try and increase the width of the input bandwidth. However, no significant improvement was seen by going above 96 Hz.

Test 14 tested a varisweep designed around the results of the previous tests.

SUMMARY (Cont'd)

The remaining tests (15-24) tested the use of the tractor vibs as compared to the buggy vibs. The data resulting from the use of the buggies was deemed to be superior and the buggy vibs were used throughout the contract.

The final parameters chosen from testing and implemented as the production parameters were as follows:

Number of Vibrators:	Three
Number of Composites:	Six
Sweep Length:	Eight seconds
Sweep Frequencies:	12-76; 12-80; 13-84; 13-88; 14-92; 14-96 Hz
Move-up Between Sweeps:	4 m
Drive Level:	30%
Listen Time:	5 seconds
Sample Rate:	2 ms

4.2 RECORDING PARAMETERS

Energy Source:	3 Vibrators on Line
Vibrator Station Interval:	30 m
Vibrator Array:	40 m
Receivers:	6 Mark L21A 10 Hz geophones per string
Receiver Interval:	6 phones over 10 m
Receiver Array:	10 m in line
Sweep Length:	8 sec.
Number of Composites:	6
Sweep Type:	Linear Up Sweep
Varisweep Frequencies:	12-76 Hz 12-80 Hz 13-84 Hz 13-88 Hz 14-92 Hz 14-96 Hz
Vibrator Drive Level:	30%
Spread Geometry:	512 Split Spread
Offset Range:	2560 - 0 - 2560
Record Length:	5 sec.
Acquisition Sample Rate:	2 m/s

4.3 RECORDING STATISTICS

ROSEDALE

LINE NUMBER	85-07	85-8	85-10	85-10A	85-10B	85-9
VP TO VP (a)	260 - 1511	162 - 1059	206 - 1847	100 - 898	100 - 823	27 - 675
GEOPHONE TO GEOPHONE (b)	260 - 1511	150 - 1060	200 - 1848	100 - 899	100 - 825	27 - 675
Nº PROFILES	409	296	543	260	236	215
Nº PROFILES SKIPPED	9	29	7	10	6	7
TOTAL KMS (a)	12.510	8.970	16.410	7.980	7.230	6.480
(b)	12.510	9.100	16.480	7.990	7.250	6.480
RECORD HOURS	19.50	15.00	25.625	15.750	11.125	11.250
TEST TIME	7.50	1.50	1.75	1.00	1.25	0.75
DOWN TIME	7.00	3.00	1.25	2.25	0.25	1.25
OTHER TIME	5.50	7.375	4.375	3.250	2.250	3.00
DATES RECORDED	3, 4, 5, 6 Jan. 1985	7, 8, 9 Jan. 1985	9, 10, 11, 12 Jan. 1985	12, 13, 14 Jan. 1985	14-15 Jan. 1985	16-17 Jan. 1985

4.3 RECORDING STATISTICS

ROSEDALE

LINE NUMBER	85-6	85-16	85-5	85-4	85-3	85-11
VP TO VP (a)	106 - 1972	829 - 100	2083 - 100	100 - 2077	2065 - 100	2050 - 94
GEOPHONE TO GEOPHONE (b)	103 - 1972	830 - 100	2086 - 100	100 - 2077	2065 - 100	2050 - 94
Nº PROFILES	622	240	661	658	653	646
Nº PROFILES SKIPPED	7	10	14	5	16	6
TOTAL KMS (a)	18.660	7.290	19.830	19.770	19.650	19.560
(b)	18.690	7.300	19.860	19.770	19.650	19.560
RECORD HOURS	26.750	10.750	28.000	25.000	28.125	23.875
TEST TIME	2.750	0.50	2.00	1.50	2.00	1.75
DOWN TIME	4.50	1.00	4.25	3.25	3.00	1.625
OTHER TIME	5.00	1.00	5.50	4.00	4.125	5.375
DATES RECORDED	17-20 Jan. 1985	21 Jan. 1984	22-25 Jan. 1985	26-28 Jan. 1985	29, 30, 31 Jan & 1 Feb. 1985	1, 2, 3, 4 Feb. 1985

4.3 RECORDING STATISTICS

ROSEDALE

LINE NUMBER	85-2	85-14	85-15	85-13	85-19	85-17
VP TO VP (a)	10 - 2053	103 - 1315	100 - 1111	1462 - 100	100 - 1051	820 - 100
GEOPHONE TO GEOPHONE (b)	10 - 2053	100 - 1315	100 - 1111	1465 - 100	100 - 1051	823 - 100
Nº PROFILES	675	403	335	455	317	242
Nº PROFILES SKIPPED	6	3	1	1	1	0
TOTAL KMS (a)	20.430	12.120	10.110	13.620	9.510	7.200
(b)	20.430	12.120	10.110	13.650	9.510	7.230
RECORD HOURS	23.375	14.750	12.625	18.000	7.250	7.875
TEST TIME	1.50	1.00	0.75	1.625	0.750	0.250
DOWN TIME	0.625	0.50	1.00	2.875	0.625	0
OTHER TIME	6.250	4.375	3.375	4.50	1.750	2.750
DATES RECORDED	4, 5, 6, 7 Feb. 1985	7, 8, 9 Feb. 1985	9-10 Feb. 1985	11, 12, 13 Feb. 1985	13-14 Feb. 1985	14-15 Feb. 1985

4.3 RECORDING STATISTICS

ROSEDALE

LINE NUMBER	85-18	85-12	85-1				
VP TO VP (a)	700 - 322	1351 - 100	1942 - 85				
GEOPHONE TO GEOPHONE (b)	700 - 322	1351 - 100	1942 - 85				
Nº PROFILES	127	416	614				
Nº PROFILES SKIPPED	0	2	5				
TOTAL KMS (a)	3.780	12.510	18.570				
(b)	3.780	12.510	18.570				
RECORD HOURS	7.375	15.375	21.375				
TEST TIME	0.375	0.875	1.625				
DOWN TIME	0.125	0.375	3.00				
OTHER TIME	3.250	5.750	11.000				
DATES RECORDED	15-16 Feb. 1985	16, 17, 18 Feb. 1985	18, 19, 20, 21 Feb. 1985				

5. FIELD PROCESSING

5.1 PROCESSING OBJECTIVES

- 1) To provide quality control of all Vibroseis acquired seismic data;
- 2) To provide quality control of all survey data;
- 3) To provide a brute stack of raw Vibroseis data on a daily basis for the client, and to provide a completed raw field stack section with the completion of each line.

5.2 PROCESSING REVIEW

Geosystems' processing of the 1985 Rosedale Seismic Survey was limited to field processing on a nightly basis, with in-house processing being performed by Geophysical Services Inc. For this reason field processing concentrated on the quality of the field stacks and fulfilling any requests made by the client, Mr. Claus Kuball, with no testing for in-house processing parameters

During the contract the listed proposals were largely fulfilled. Co-ordinate tapes were created for Lines GHG85A-03, 05, 06, 07, 08, 09, 10, 10A, 10B and 16 as survey data was made available. These co-ordinate tapes contained ground co-ordinate and elevation information and were used to check the quality of survey data by producing a hard copy dump of the co-ordinates for each shot/receiver point on a line, as well as a survey map and elevation profile of each line.

Processing parameters (front mutes and velocity functions) were chosen as often as processing time allowed, with the interval between new sets of parameters approximately 6 km.

Using the chosen parameters, the raw Vibroseis data and, when available, co-ordinate/elevation data, each line was stacked to a two-way time of 3 seconds. Lines GHG85A- 05, 06, 09, 10, 10A and 10B were stacked with real co-ordinates and elevations, which

5.2 PROCESSING REVIEW (Cont'd)

allowed elevation statics to be applied to these lines, but all other lines were stacked with dummy co-ordinates, so no correction could be made for elevation variations.

Processing Results

In general all stacked lines showed high resolution of seismic reflectors from depths of 0.1 - 0.2 to 1.0 - 1.5 seconds, displaying strong coherency of high frequency data. An area of poor quality data was encountered in the North-West of the prospect and this badly affected sections of data on Lines GHG85A-01, 02, 03 and 11.

In the case of Line GHG85A-02, the sudden marked change in data quality resulted in a front mute being too wide, allowing refraction data into the stack over a range of approximately thirty C.D.P.'s. To remove this, velocity filter tests were run and a velocity of 1900 m/sec was chosen to filter the line. The result was complete removal of the refractions and slight enhancement of shallow reflectors on the line.

In an attempt to enhance data in the North of line GHG85A-01, tests were run using the Differential Field Sum Program (DFS). This program allows a small geophone array to be used during acquisition and a longer array to be synthesised by the Geocor IV, while at the same time applying a partial NMO correction to the data to compensate for offset differences. The use of a small receiver array in the field allows more accurate static correction calculation, as well as attenuating short wavelength coherent noise, while longer computer simulated arrays are more competent at removing longer wavelength noise such as groundroll. The overall effect is enhanced coherency of seismic reflectors and the breakdown of noise interference.

After the tests had been run, 8 x 3 D.F.S. (80 metre synthesised array) was chosen and applied to field files 480 to 600. These

Processing Results (Cont'd)

files were then stacked to a depth of 2 seconds with 15 metre C.D.P. intervals. Unfortunately, there was negligible improvement of data in the poor quality data region, although there was improvement of reflector coherency to the far North of the line where data quality was already good.

5.3 SUMMARY

The results of field processing were generally very encouraging with the raw field stacks giving a clear indication of the geological structure of the survey area. This resulted in the inclusion of several extra survey lines, GHG85A-12, 13, 14, 15, 17, 18 and 19 in order to increase coverage of interesting structural features.

6. PERSONNEL MOVEMENTS

6.1 PERSONNEL

2 Party Managers	-	P. Jamieson, H. Athorn
1 Assistant Party Manager	-	S. Barbour
2 Processors	-	C. Luxton, B. Hipkiss
2 Observers	-	R. Permann, H. Hume
1 Junior Observer	-	S. Jeyaseelan
3 Surveyors	-	J. Meggitt, T. Newmair, R. Losier
2 Vibrator Technicians	-	P. Kilpatrick, B. Grimes
1 Mechanic	-	G. Rafferty
5 Vibe Operators	-	B. Darch, L. Dean, J. Fing, B. Wilgosh, S. Whalley
24 Field Assistants		

6.2 CLIENT AND NON-BASIC FIELD CREW PERSONNEL

2	January	-	F. O'Sullivan arrives
4	"	-	" " leaves
18	"	-	F. O'Sullivan arrives
17	"	-	Dan Scanlon arrives
20	"	-	Dan Scanlon leaves
25	"	-	J. Rae arrives
30	"	-	S. Greaves, Hartogen, arrives
31	"	-	J. Rae, D. Scanlon leave

APPENDIX "A"

TECHNICAL EQUIPMENT

- Two hundred and one (201) geophone cables, each eight hundred and eighty (880) feet long with takeouts spaced at one hundred and ten (110) feet.
- Sixteen (16) jumper cables two hundred (200) feet long.
- Fourteen hundred and one (1401) geophone strings with six (6) Mark L-21A 10 hz geophones per string spaced at thirty (30) foot intervals.
- Assorted test equipment such as Techtronic scope, Geophone tester and simulator, cable checkers, line simulator, volt meters and etc.
- Twelve (12) Motorola radios for communications.
- Eight (8) repeater terminals.
- Array terminal repair station.
- One hundred and seven (107) array terminals, and necessary amount of battery chargers.
- Two (2) Wild T16 Theodolites.
- Two (2) Sokkisha Auto Ranger Systems.
- Geocor IV 1024 channel seismic data acquisition and processing system. Mounted within an air-conditioned cab on an F-700 four wheel drive truck.
- Four (4) Litton LRS 311 vibrators mounted on International Paystar 5000 six-wheel trucks equipped with Pelton vibrator electronics.
- One vibrator service Isuzu four wheel drive unit.
- Two cable and geophone Isuzu four wheel drive units.
- Two array terminal Toyota vehicles.
- Seven field Toyotas.
- One Isuzu, six-wheel truck mounted with fire fighting equipment.
- Three Isuzu four wheel transport trucks.
- One 12 channel OYO McSeis 1500 refraction system.
- One 24 channel TR7 Field-ographs uphole refraction system.
- One 1340, 24 channel Field-ograph uphole refraction system.
- Two Toyota four wheel drive shooting/preloading vehicles.

APPENDIX "B"

SURVEY STATISTICS

LINE N°: GHG 85A-01
TERRAIN: Undulating - Pine Plantations, 4.0 kms
START OF LINE: VP 85
END OF LINE: VP 1942
TOTAL KMS: 18.57
TOTAL PM's: 3
SURVEY PROCEDURE: Start of survey VP 85 - traverse North to South
end of survey VP 1942.
UNUSUAL OCCURRENCES: 4.0 kms was cut through Pine Plantations by
D-6 Dozer.

LINE N°: GHG 85A-02
TERRAIN: Undulating - Pine Plantations 5.0 kms
START OF LINE: VP 10
END OF LINE: VP 2053
TOTAL KMS: 20.43
TOTAL PM's: 6
SURVEY PROCEDURE: Start of survey VP 10 traverse North to South,
end of survey VP 2053.
UNUSUAL OCCURRENCES: 5.0 kms was cut through Pine Plantations by
D-6 Dozer.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-03
TERRAIN: Undulating, pine plantations and some forrest
4.0 kms
START OF LINE: VP 100
END OF LINE: VP 2065
TOTAL KMS: 19.65
TOTAL PM's: 4
SURVEY PROCEDURE: Start of survey VP 100 traverse North to South
end of survey VP 2065 tie to Line 85A-04 VP 2077.
UNUSUAL OCCURRENCES: 4.0 kms was cut through pine plantation and
forrest by D-6 Dozer.

LINE N°: GHG 85A-04
TERRAIN: Mostly flat, some parts heavy trees and pine
plantation 3.0 kms
START OF LINE: VP 100
END OF LINE: VP 2077
TOTAL KMS: 19.77
TOTAL PM's: 3
SURVEY PROCEDURE: Start of survey VP 100 traverse North to South
end of survey VP 2077.
UNUSUAL OCCURRENCES: 3.0 kms was cut by D-6 Dozer through heavy
trees and pine forrest.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-05
TERRAIN: Flat with some clearing through forrest and
scrub 5.0 kms
START OF LINE: VP 100
END OF LINE: VP 2086
TOTAL KMS: 19.86
TOTAL PM's: 5
SURVEY PROCEDURE: Start of survey VP 100 traverse North to South
end of survey VP 2086.
UNUSUAL OCCURRENCES: 5.0 kms was cut by D-6 Dozer through rain forrest
and pine plantations.

LINE N°: GHG 85A-06
TERRAIN: Mostly flat, pine forrest and rain forrest to the
South 8.0 kms
START OF LINE: VP 103
END OF LINE: VP 1972
TOTAL KMS: 18.69
TOTAL PM's: 4
SURVEY PROCEDURE: Start of survey VP 103 traverse North to South
end of survey VP 1972 tie to Line 16 VP 797 + 4.
UNUSUAL OCCURRENCES: Dozer cut 8.0 kms through rain forrest and pine
plantations.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-07
TERRAIN: Mostly flat - rain forrest and pine plantations
5.5 kms
START OF LINE: VP 262
END OF LINE: VP 1511
TOTAL KMS: 12.49
TOTAL PM's: 3
SURVEY PROCEDURE: Start of survey VP 262 traverse North to South
end of survey VP 1511.
UNUSUAL OCCURRENCES: 5.5 kms was cut by D-6 Dozer through pine
plantations and rain forrest.

LINE N°: GHG 85A-08
TERRAIN: Flat open country, marsh flats to the North
START OF LINE: VP 150
END OF LINE: VP 1060
TOTAL KMS: 9.10
TOTAL PM's: 2
SURVEY PROCEDURE: Start of survey VP 150 traverse North to
South to VP 1060 E.O.L.
UNUSUAL OCCURRENCES: None.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-09
TERRAIN: Marshes to the North and South, flat open ground
medium scrub
START OF LINE: VP 27
END OF LINE: VP 675
TOTAL KMS: 6.48
TOTAL PM's: 4
SURVEY PROCEDURE: Surveyed from Line 10B to the South to VP 675
E.O.L. from VP 466 + 5 to the North to VP 27
S.O.L.
UNUSUAL OCCURRENCES: 4.5 kms cleared with D-3 Dozer.

LINE N°: GHG 85A-10
TERRAIN: Mostly flat follows Longford Road
START OF LINE: VP 200
END OF LINE: VP 1848 + 8
TOTAL KMS: 16.56
TOTAL PM's: 4
SURVEY PROCEDURE: Start of survey VP 200 traverse West to East to
VP 1848 + 8 E.O.L.
UNUSUAL OCCURRENCES: None.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-10A
TERRAIN: Undulating with marshes to the East and middle
of line
START OF LINE: VP 100
END OF LINE: VP 900
TOTAL KMS: 8.00
TOTAL PM's: 3
SURVEY PROCEDURE: Start of survey VP 100 traverse West to East
to VP 900 E.O.L.
UNUSUAL OCCURRENCES: None.

LINE N°: GHG 85A-10B
TERRAIN: Flat with marshes along the line
START OF LINE: VP 100
END OF LINE: VP 825
TOTAL KMS: 7.25
TOTAL PM's: 4
SURVEY PROCEDURE: Start of survey VP 100 traverse West to East
to VP 825 E.O.L.
UNUSUAL OCCURRENCES: Dozed 1.0 kms with D-3 Dozer.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-11
TERRAIN: Undulating to very hilly at Boundary Creek
area
START OF LINE: VP 94
END OF LINE: VP 2050
TOTAL KMS: 19.56
TOTAL PM's: 5
SURVEY PROCEDURE: Start of survey VP 2050 E.O.L. traverse East
to West to VP 94 S.O.L.
UNUSUAL OCCURRENCES: 6.0 kms dozing with D-6 through hills.

LINE N°: GHG 85A-12
TERRAIN: Mostly undulating
START OF LINE: VP 100
END OF LINE: VP 1351
TOTAL KMS: 12.51
TOTAL PM's: 2
SURVEY PROCEDURE: Start of survey VP 1351 E.O.L. traverse East
to West to VP 100 S.O.L.
UNUSUAL OCCURRENCES: 1.0 kms cleared with D-6 Dozer.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-13
TERRAIN: Undulating - pine plantation rain forrest
START OF LINE: VP 100
END OF LINE: VP 1465
TOTAL KMS: 13.65
TOTAL PM's: 2
SURVEY PROCEDURE: Surveyed from VP 100 S.O.L. traversed West to East to VP 1465 E.O.L.
UNUSUAL OCCURRENCES: Line cleared for 2.0 kms D-6.

LINE N°: GHG 85A-14
TERRAIN: Partly flat to undulating
START OF LINE: VP 100
END OF LINE: VP 1315
TOTAL KMS: 12.15
TOTAL PM's: 5
SURVEY PROCEDURE: Surveyed West to East from VP 100 S.O.L. to VP 1315 E.O.L.
UNUSUAL OCCURRENCES: Dozed 1.0 kms D-6.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-15
TERRAIN: Undulating to flat in parts.
START OF LINE: VP 100
END OF LINE: VP 1111
TOTAL KMS: 10.11
TOTAL PM's: 4
SURVEY PROCEDURE: Start of survey VP 1111 E.O.L. traverse East
to West to VP 100 E.O.L.
UNUSUAL OCCURRENCES: Dozed 1.0 kms through forrest.

LINE N°: GHG 85A-16
TERRAIN: Undulating to flat in parts
START OF LINE: VP 100
END OF LINE: VP 830
TOTAL KMS: 7.30
TOTAL PM's: 2
SURVEY PROCEDURE: Start VP 100 traverse North - South to VP 830
E.O.L.
UNUSUAL OCCURRENCES: 3.5 kms dozed through pine plantation D-6.

SURVEY STATISTICS (Cont'd)

LINE N°: GHG 85A-17
TERRAIN: Flat follows fenceline
START OF LINE: VP 100
END OF LINE: VP 823
TOTAL KMS: 7.23
TOTAL PM's: 4
SURVEY PROCEDURE: Surveyed from VP 100 North - South to VP 823
E.O.L.
UNUSUAL OCCURRENCES: None.

LINE N°: GHG 85A-18
TERRAIN: Undulating with marshes to the South E.O.L.
START OF LINE: VP 322
END OF LINE: VP 700
TOTAL KMS: 3.78
TOTAL PM's: 1
SURVEY PROCEDURE: Survey starts at VP 322 S.O.L. North - South
to VP 700 E.O.L.
UNUSUAL OCCURRENCES: Dozed 0.5 kms with D-6.

SURVEY STATISTICS (Cont'd)

LINE N°:	GHG 85A-19
TERRAIN:	Flat open grazing land
START OF LINE:	VP 100
END OF LINE:	VP 1051
TOTAL KMS:	9.51
TOTAL PM's:	3
SURVEY PROCEDURE:	Start of survey VP 100 S.O.L. from West to East to VP 1051 E.O.L.
UNUSUAL OCCURRENCES:	None.

APPENDIX "C"

LIST OF PERMANENT MARKERS

APPENDIX "D"

LIST OF DATA TAPES (ROSEDALE)

<u>TAPE N°</u>	<u>FILE N°</u>	<u>VP N°</u>
<u>LINE 85-07</u>		
TEST TAPE HELTEST-01	1 - 14	515
" " HELTEST-02	15 - 24	515
TAPE GHGFA 001 - 009	1 - 139	260 - 692
010 - 019	140 - 298	695 - 1169
020 - 026	299 - 409	1172 - 1511
<u>LINE 85-08</u>		
TAPE GHGFA 027 - 029	1 - 48	162 - 303
030 - 039	49 - 205	303 - 786
040 - 047	206 - 296	789 - 1059
<u>LINE 85-10</u>		
TAPE GHGFA 048 - 049	1 - 32	206 - 293
050 - 059	33 - 178	296 - 749
060 - 069	179 - 335	752 - 1223
070 - 079	336 - 490	1226 - 1688
080 - 083	491 - 543	1691 - 1847
<u>LINE 85-10A</u>		
TAPE GHGFA 084 - 089	1 - 97	100 - 394
090 - 100	98 - 260	397 - 898
<u>LINE 85-10B</u>		
TAPE GHGFA 101 - 109	1 - 143	100 - 538
110 - 116	144 - 236	541 - 823
<u>LINE 85-09</u>		
TAPE GHGFA 117 - 119	1 - 48	27 - 168
120 - 131	49 - 215	171 - 675

LIST OF DATA TAPES (ROSEDALE) (Cont'd)

<u>TAPE N°</u>	<u>FILE N°</u>	<u>VP N°</u>
<u>LINE 85-06</u>		
TAPE GHGFA 132 - 139	2 - 128	106 - 484
140 - 149	129 - 288	487 - 964
150 - 159	289 - 448	967 - 1444
160 - 172	449 - 622	1447 - 1972
<u>LINE 85-16</u>		
TAPE GHGFA 173 - 179	1 - 97	829 - 541
180 - 191	98 - 240	538 - 100
<u>LINE 85-05</u>		
TAPE GHGFA 192 - 199	1 - 116	2083 - 1741
200 - 209	117 - 251	1738 - 1333
210 - 219	252 - 400	1330 - 886
220 - 229	401 - 559	886 - 406
230 - 236	560 - 661	403 - 100
<u>LINE 85-04</u>		
TAPE GHGFA 237 - 239	1 - 48	100 - 244
240 - 249	49 - 208	247 - 727
250 - 259	209 - 368	730 - 1207
260 - 269	369 - 528	1210 - 1687
270 - 278	529 - 658	1690 - 2077
<u>LINE 85-03</u>		
TAPE GHGFA 279 - 289	1 - 168	2065 - 1564
290 - 299	169 - 328	1561 - 1084
300 - 309	329 - 478	1081 - 625
310 - 320	479 - 653	622 - 100

LIST OF DATA TAPES (ROSEDALE) (Cont'd)

<u>TAPE N°</u>	<u>FILE N°</u>	<u>VP N°</u>
<u>LINE 85-11</u>		
TAPE GHGFA 321 - 329	1 - 133	2050 - 1648
330 - 339	134 - 288	1645 - 1180
340 - 349	289 - 432	1177 - 745
350 - 359	433 - 592	742 - 262
360 - 363	593 - 646	259 - 94
<u>LINE 85-02</u>		
TAPE GHGFA 364 - 369	1 - 94	10 - 292
370 - 379	95 - 221	295 - 676
380 - 389	222 - 379	679 - 1159
390 - 399	380 - 538	1162 - 1639
400 - 409	539 - 675	1642 - 2053
<u>LINE 85-14</u>		
TAPE GHGFA 410 - 419	1 - 157	103 - 571
420 - 429	158 - 318	574 - 1060
430 - 435	319 - 403	1063 - 1315
<u>LINE 85-15</u>		
TAPE GHGFA 436 - 439	1 - 64	100 - 289
440 - 449	65 - 224	292 - 778
450 - 457	225 - 335	781 - 1111
<u>LINE 85-13</u>		
TAPE GHGFA 458 - 459	1 - 32	1462 - 1372
460 - 469	33 - 179	1369 - 931
470 - 479	180 - 339	928 - 451
480 - 487	340 - 455	448 - 100
<u>LINE 85-19</u>		
TAPE GHGFA 488 - 499	1 - 192	100 - 676
500 - 508	193 - 317	679 - 1051

LIST OF DATA TAPES (ROSEDALE) (Cont'd)

<u>TAPE N°</u>	<u>FILE N°</u>	<u>VP N°</u>
<u>LINE 85-17</u>		
TAPE GHGFA 509 - 519	1 - 157	820 - 355
520 - 525	158 - 242	352 - 100
<u>LINE 85-18</u>		
TAPE GHGFA 526 - 531	1 - 127	700 - 322
<u>LINE 85-12</u>		
TAPE GHGFA 532 - 539	1 - 118	1351 - 994
540 - 549	119 - 263	991 - 559
550 - 559	264 - 416	556 - 100
<u>LINE 85-01</u>		
TAPE GHGFA 560 - 569	1 - 145	1942 - 1504
570 - 579	146 - 299	1501 - 1042
580 - 589	300 - 450	1039 - 583
590 - 600	451 - 614	580 - 85

APPENDIX B

GEOCOR IV

SEISMIC DATA ACQUISITION AND PROCESSING SYSTEM

FIELD TAPE FORMAT

(May 3, 1979)

GEOPHYSICAL SYSTEMS CORPORATION
2085 EAST FOOTHILL BOULEVARD
PASADENA, CALIFORNIA, 91107

GEOCOR IV

FIELD TAPE FORMAT

Field data is recorded on IBM compatible $\frac{1}{2}$ inch, 9 track tape in demultiplexed format at either 800 or 1600 bits-per-inch density. Each tape reel is divided into trace data blocks each containing a trace identification header and data values from one channel (Fig. 1). Each trace data block is separated from the next by a .6 inch interblock gap (IBG). Data values are recorded in two's complement notation with 16 bits per sample standard (recording 1 or 8 bits per sample is available as a non-standard option).

Two trace data block formats are available:

Trace Data Block - 4 word Trace Identification Header (Fig. 2)
Format #1

Trace Data Block - 32 word Trace Identification Header (Fig. 3)
Format #2

Trace Data Block Format #2 contains more header information and is standard.

TRACE HEADER ITEM DEFINITIONS

	<u>Format</u>	<u>Limits</u>
File number is the sequential number assigned to each record (or file) on a magnetic tape. Each line of receivers generates one record at each source point. A record may contain from one to 1024 traces. The file numbering begins at one for the first record on the first tape and continues sequentially through all the tapes for the line.	16 bit two's complement	1 to 32767
Trace Number is the sequential number, beginning at 1, assigned to each trace collected at a source point.	16 bit two's complement	1 to 1024
Source Point Number represents the actual number assigned to each source point by the surveyor.	16 bit two's complement	-32767 to 32767
Port/Channel Code is a code identifying the input port and channel used to collect each trace. The most significant 6 bits represent the port (0-15) and the least significant 10 bits represent the channel (0-1023).	6 bit/10 bit	0-15/0-1023
Source Line Name is the alphabetic or numeric identification of the line of source points.	6 ASCII characters left justified.	
Receiver Line Name is the alphabetic or numeric identification of the line of receivers.	6 ASCII characters left justified.	
Receiver Number represents the actual number assigned to each receiver location by the surveyor.	16 bit two's complement	-32767 to 32767

GEOCOR IV
FIELD TAPE FORMAT

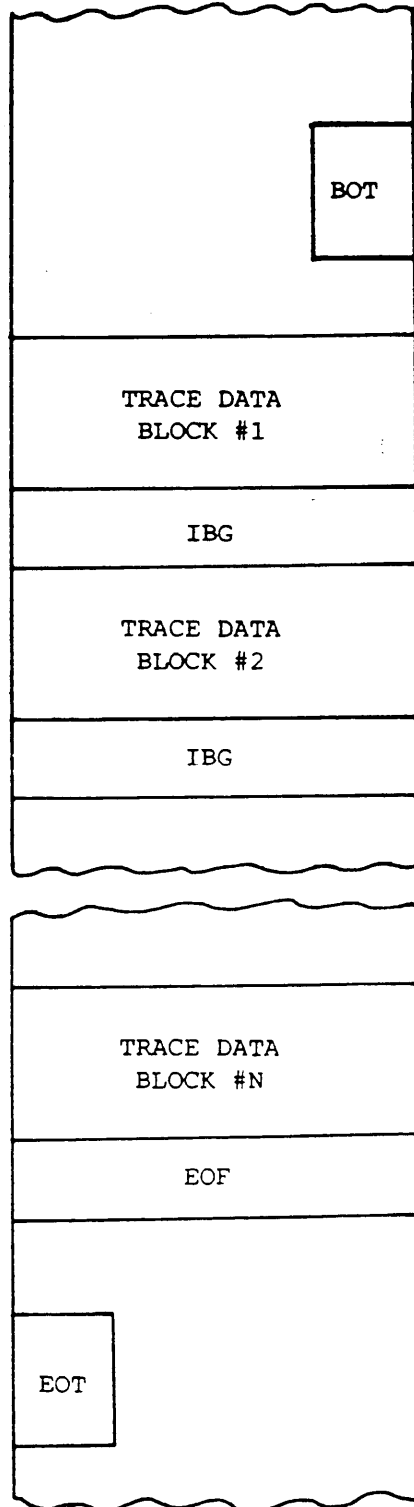


FIG. 1

FORMAT #1
TRACE DATA BLOCK

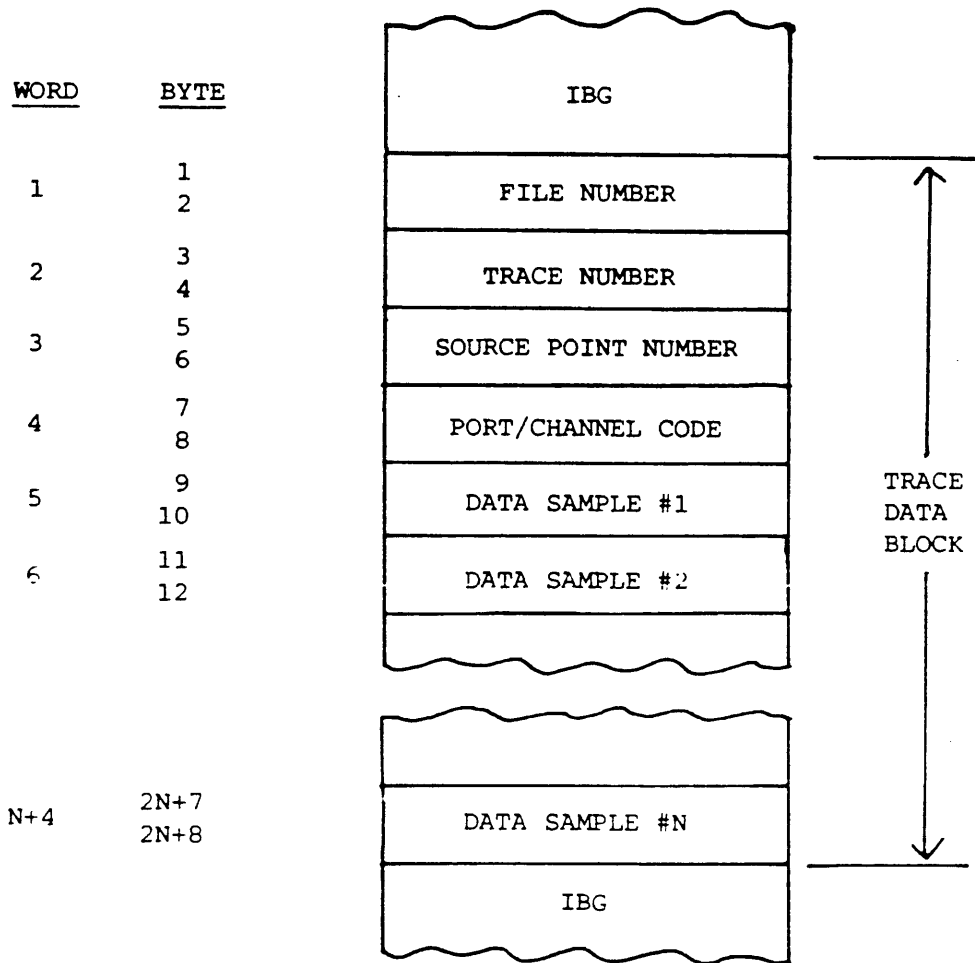


FIG. 2

TRACE DATA BLOCK FORMAT #2

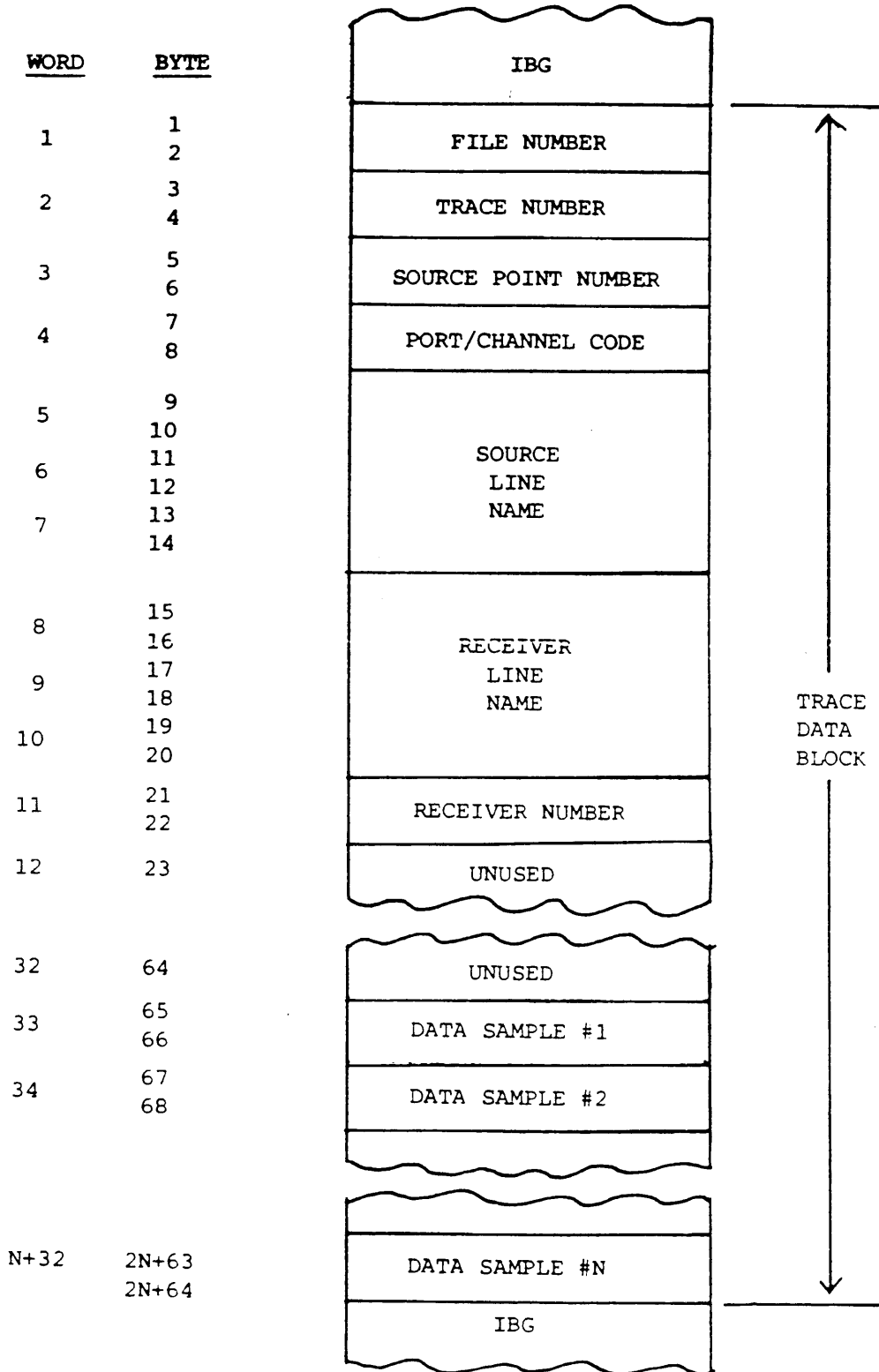


FIG. 3

STACK TAPE FORMAT

<u>WORD</u>	<u>CONTENTS</u>
1	File
2	Trace (=1) (Not Used)
23	Avg X
24	Avg X
25	Avg Y
26	Avg Y
27	Avg Static
28	Avg Weight
29	RCP X
30	RCP X
31	RCP Y
32	RCP Y

GATHER TRACE FORMAT

<u>WORD</u>	<u>BYTE</u>	
1	1-2	File Number
2	3-4	Trace Number
3	5-6	Source Point Number
4	7-8	Port/Channel Code
5-7	9-14	Source Line Name
8-10	15-20	Receiver Line Name
11	21-22	Receiver Number
12-13	23-26	Source X
14-15	27-30	Source Y
16	31-32	Source Elevation
17	33-34	Source Residual
18-19	35-38	Receiver X
20-21	39-42	Receiver Y
22	43-44	Receiver Elevation
23	45-46	Receiver Residual
33-n	65-2n	Data Samples

GEOCOR IV
SEISMIC DATA ACQUISITION AND PROCESSING SYSTEM

LOG TAPE FORMAT

(May 15, 1979)

GEOPHYSICAL SYSTEMS CORPORATION
2085 EAST FOOTHILL BOULEVARD
PASADENA, CALIFORNIA, 91107

GEOCOR IV

LOG TAPE FORMAT

All acquisition parameters and log entries recorded in the GEOCOR IV Acquisition Log may also be recorded on magnetic tape for input to subsequent data processing steps. Each line of text written in the log may be recorded as a 65-word block on tape. The format of each text block is described in Figure 2.

Information describing each source point as it is acquired is also recorded in a second format (figures 3, 4, 5). Each source point generates one block of information which contains one section describing the source location and identification and sixteen sections describing the receiver configurations. The source point blocks are 501 words long with the source section occupying words 2-101 and the receiver sections occupying words 102-501. One receiver section is filled in for each independent line of active receivers. An illustration of the total log tape is shown in figure 1.

The information is recorded on IBM compatible, $\frac{1}{2}$ inch, 9-track magnetic tape at either 800 or 1600 bits-per-inch density. Each block of information is separated from the next by a .6 inch inter-block gap (IBG). The source point blocks are written on tape in triplicate to insure that they can be read correctly. Each source point block contains a checksum word to permit detection of incorrect reads.

DEFINITIONS

	<u>Format</u>	<u>Limits</u>
Source Point Number - the number assigned to the actual ground location of each shot or vibrator point.	16 bit two's complement	-32767 to 32767
Source Line Name - the alphabetic or numeric identification of the line of source points.	6 ASCII characters left justified	
Number of Receiver Lines - the number of independent lines of receivers active during data acquisition.	16 bit two's complement	1 to 16
Checksum - the exclusive-or checksum of all the data within the block.	16 bit two's complement	-32768 to 32767
File Number - the number assigned to each group of traces generated by a line of receivers. The file numbers are sequential on tape.	16 bit two's complement	1 to 32767
Receiver Line Name - the alphabetic or numeric identification of the line of receivers.	6 ASCII characters left justified	
Reel Identification - the alphabetic or numeric identification of the magnetic tape reel.	10 ASCII characters left justified	
Number of First Active Trace - the number of the first trace containing seismic data.	16 bit two's complement	1 to 1025
Receiver Number of First Active Trace - the number assigned to the receiver location of the first active tract.	16 bit two's complement	-32767 to 32767
Number of Last Active Trace - the number of the last trace containing seismic data.	16 bit two's complement	1 to 1025
Receiver Number of Last Active Trace - the number assigned to the receiver location of the last active trace.	16 bit two's complement	-32767 to 32767
Number of Traces/File - the number of active and dummy traces within each file on tape. The number of traces/file does not change within a line.	16 bit two's complement	1 to 1025
Block Identification Code - the number which identifies the type of block. 0 = Source Point Block 1 = Text Block	16 bit two's complement	0 to 1

LOG TAPE

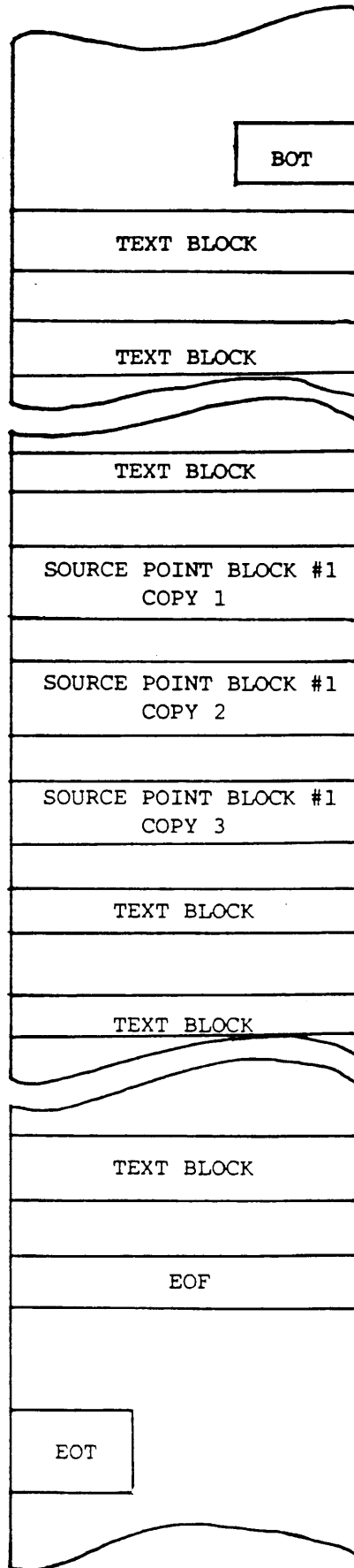


FIG. 1

TEXT BLOCK

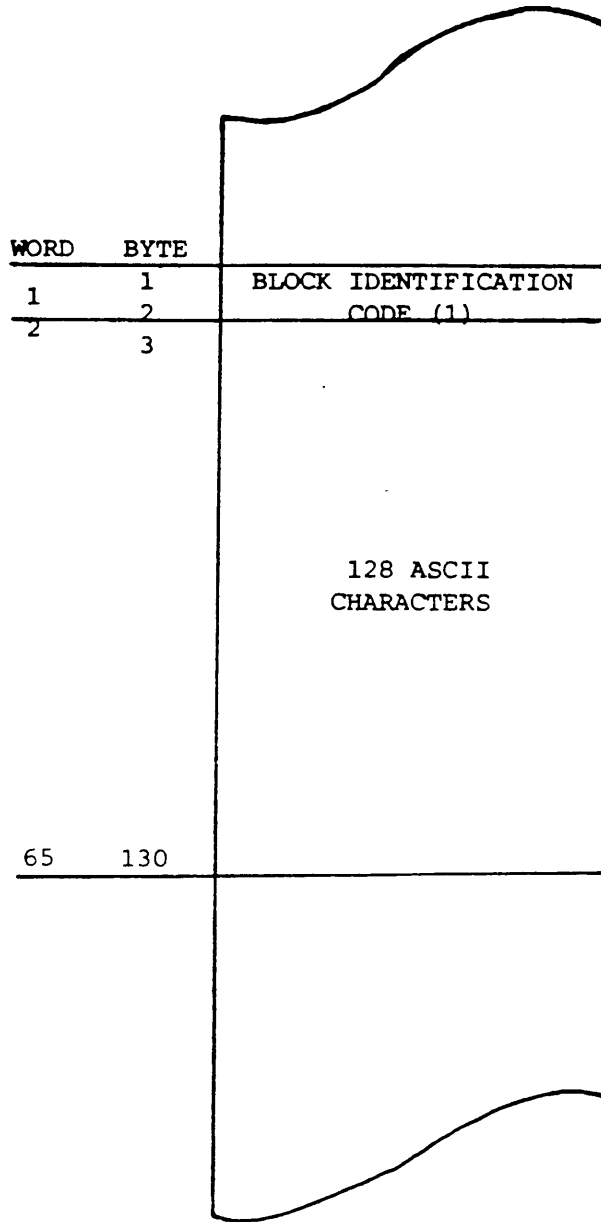


FIG. 2

SOURCE POINT BLOCK

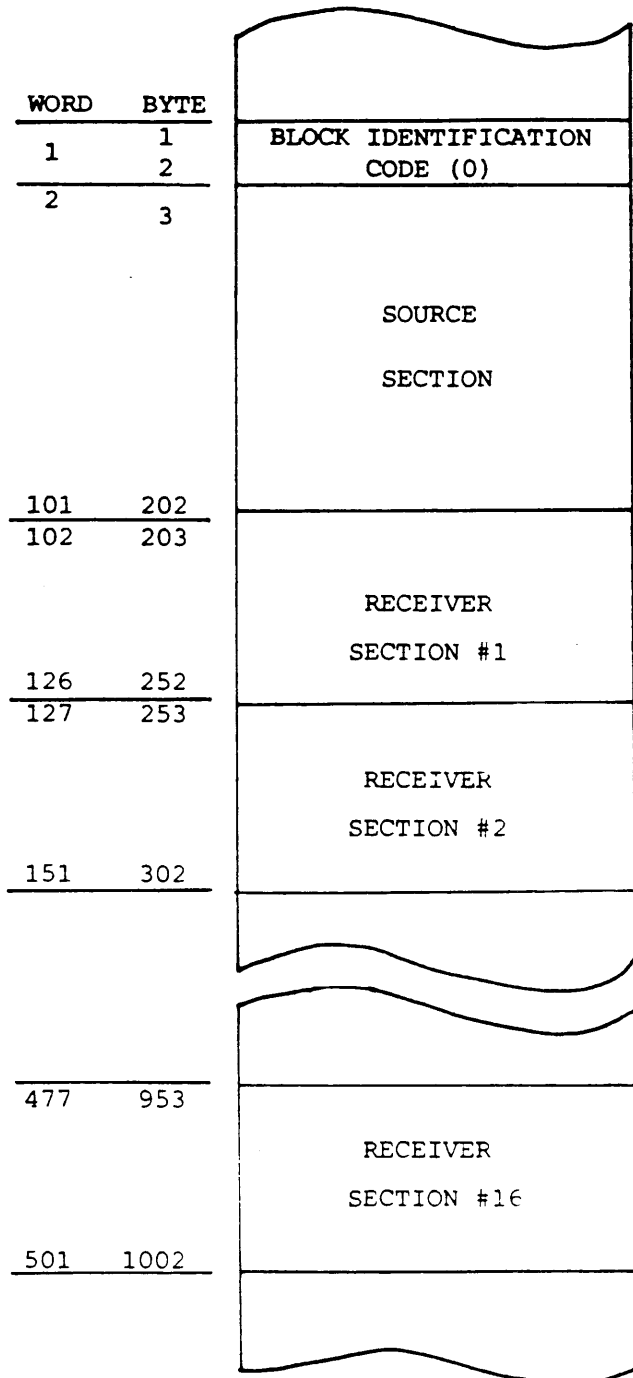


FIG. 3

SOURCE SECTION
OF SOURCE POINT BLOCK

<u>WORD</u>	<u>BYTE</u>
2	3
	4
3	5
5	10
6	11
	12
7	13
	14
8	15

100	200
101	201
	202

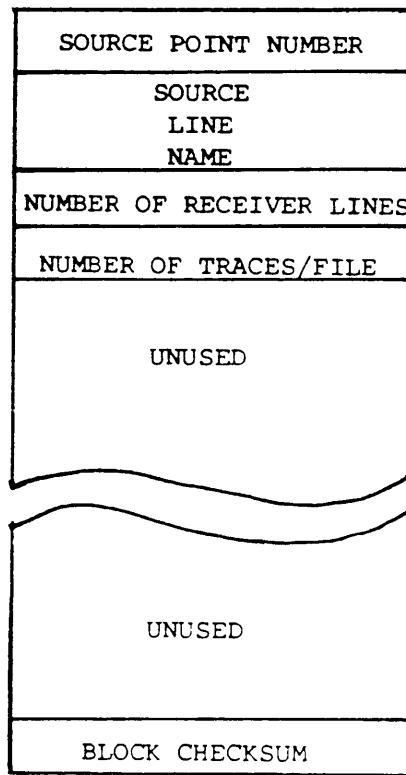


FIG. 4

RECEIVER SECTION #1
OF SOURCE POINT BLOCK

<u>WORD</u>	<u>BYTE</u>
102	203
103	204
105	210
106	211
110	220
111	221
112	223
113	225
114	227
115	229
126	252

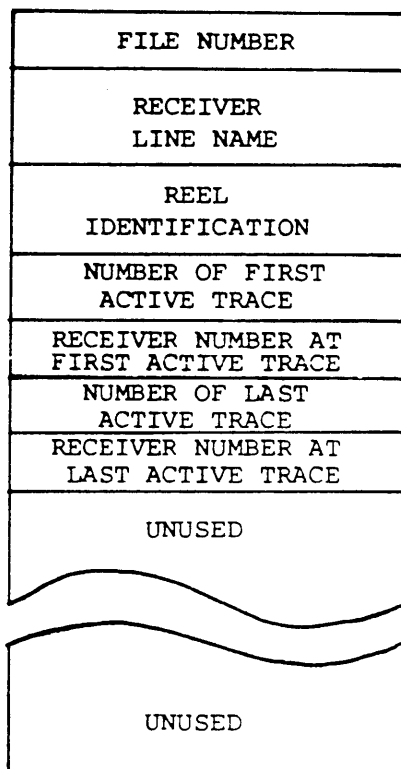


FIG. 5

GEOCOR IV

SEISMIC DATA ACQUISITION AND PROCESSING SYSTEM

COORDINATE TAPE FORMAT

(PRELIMINARY WRITEUP)

GEOPHYSICAL SYSTEMS CORPORATION
2085 EAST FOOTHILL BOULEVARD
PASADENA, CALIFORNIA, 91107

GEOCOR IV

Coordinate Tape Format

The GEOCOR IV System records geophysical survey information on magnetic tape in a blocked, gapped format which is fully IBM compatible. For each source point and receiver location associated with the survey, X, Y, and Z coordinate, residual static correction, latitude and longitude information is included. This information is recorded in data blocks which are followed on the coordinate tape by edit blocks which include receiver edit information for each source point.

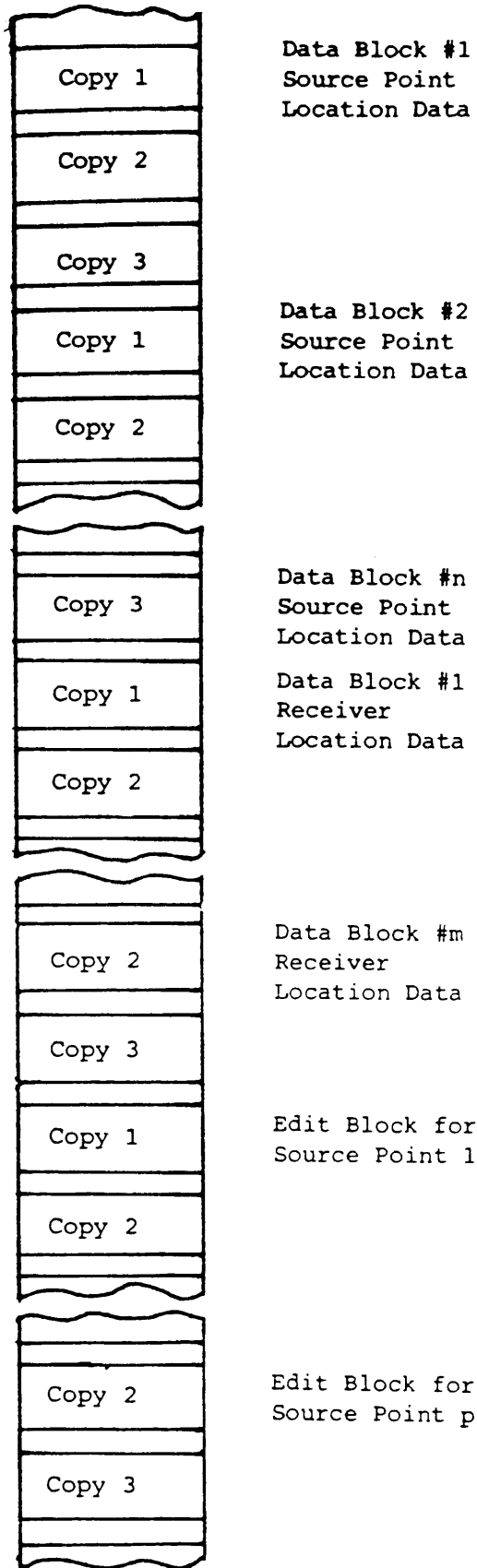
The tape is an IBM-compatible 9-track-magnetic tape that is recorded at either 800 or 1600 bits-per-inch (BPI). Tape codes consist of 16-bit words which include a sign bit and 15 data bits. The data bits are recorded in a straight binary code with a two's complement negative number representation. The sign bit of the least significant word of two word values is always set to zero.

The coordinate tape is written with three identical copies of each block. Each block is separated from the next block by a .6 inch interblock gap (IBG). Data blocks contain 2002 words each and edit blocks contain 1040 words each. (Fig. 1).

Each data block contains a block number (word 1), 100 20-word records (words 2-2001) and a checksum (word 2002). (Fig. 2). Each 20-word record is associated with a source point or receiver location. Latitude and longitude are expressed in hundredths of a second as 32-bit integer values. (Fig. 3).

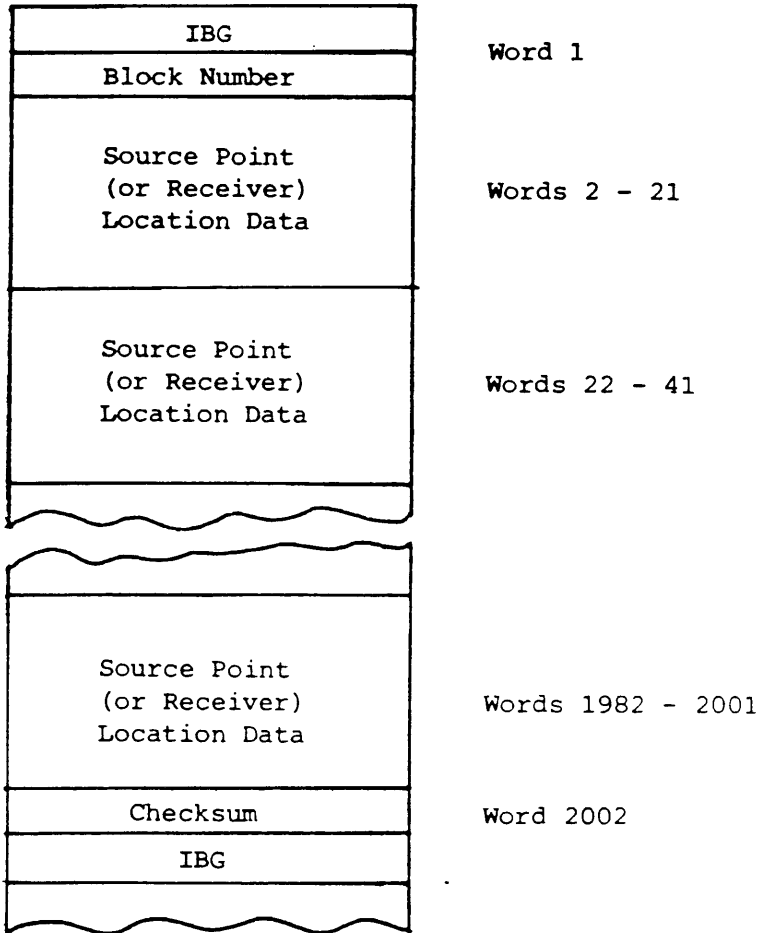
Each edit block contains a block number (word 1), the source point number to which the edits apply (word 2), the number of receiver edits included in the block (word 3), spare words (words 4-15), receiver edits (words 16-1039) and a checksum (word 1040). (Fig. 4).

The first n blocks on the coordinate tape contain source point location data and are numbered consecutively from 1 to n. These are followed by m blocks containing receiver location data numbered from 1 to m. An all-zero record indicates the termination of data within a block, and the remainder of the records in that block will also be all-zero. These data blocks are followed by p edit blocks numbered consecutively from 1 to p. There is one 1040-word edit block for each source point described in the first n data blocks.



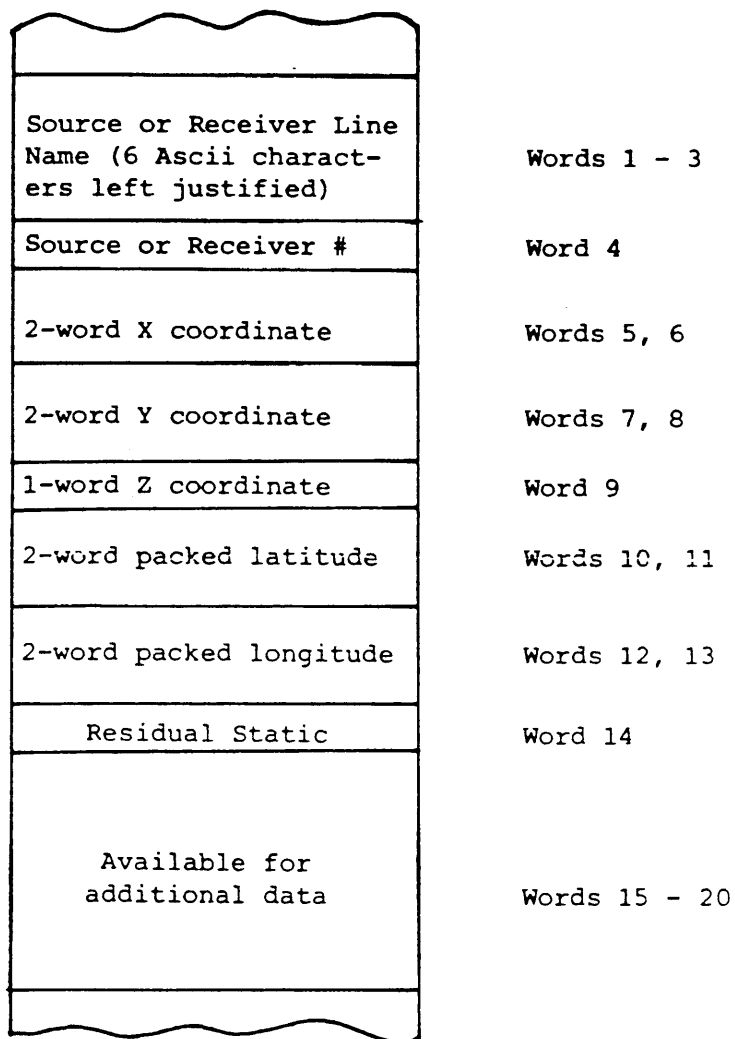
COORDINATE TAPE FORMAT

FIG. 1



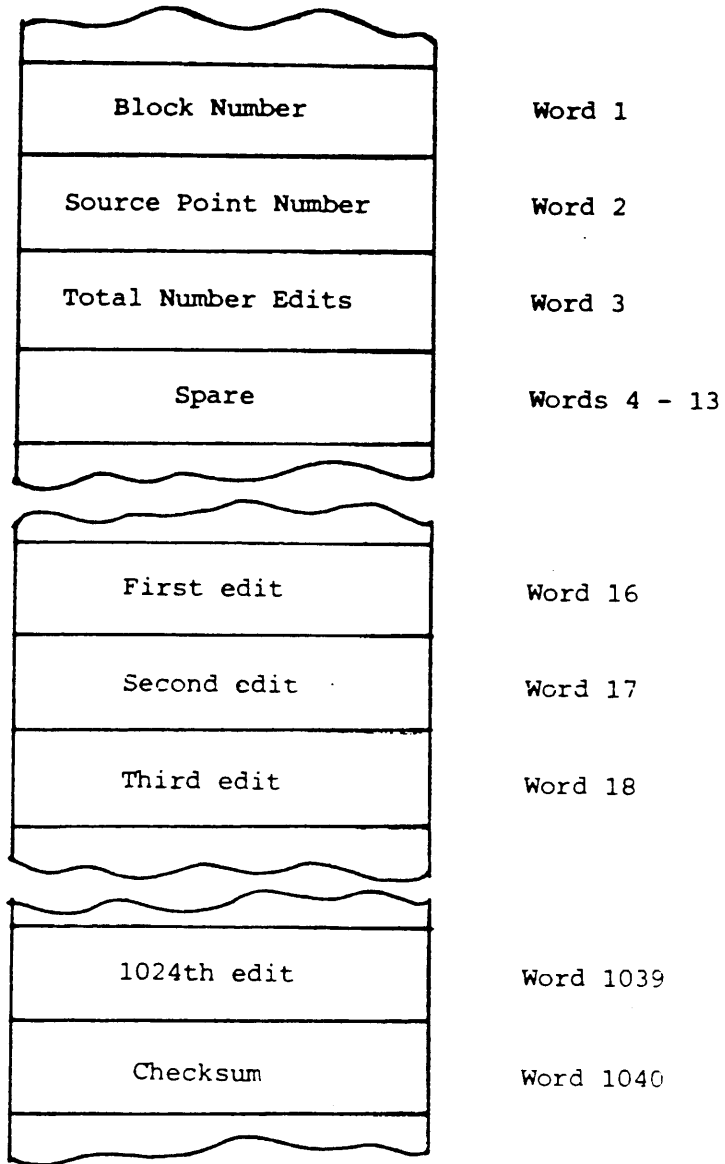
BLOCK FORMAT

FIG. 2



DATA RECORD FORMAT

FIG. 3



EDIT BLOCK FORMAT

FIG. 4

RESIDUAL TAPE FORMAT

The raw residuals output by TDR100 are stored on magnetic tape in variable length records (not longer than 2055 16-bit words). Each source or receiver line is split into segments not exceeding 2048 residual points worth of data. Each record on tape (described below) includes either the raw residuals or correlation counts for one segment and is output in triplicate. The block numbers for residuals are increasing positive integers, while the correlation blocks immediately follow and are numbered with the additive inverse of the corresponding residual block.

All source lines are present on the residual tape before the receiver lines, and the coordinate tape information is used to differentiate the source and receiver records.

For example, a typical 3D prospect might include:

	<u>LINE NAME</u>	<u>POINTS</u>
Source	SRC001	1 - 3500
	SRC002	5001 - 6000
Receiver	REC001	1 - 256
	REC002	1001 - 1256

This would produce a residual output tape as follows:

<u>BLOCK</u>	<u>CONTENT</u>	(Each block in triplicate)	
1	SRC001	1 - 2048	Raw residuals
-1	SRC001	1 - 2048	Correlation count
2	SRC001	2049 - 3500	Raw residuals
-2	SRC001	2049 - 3500	Correlation count
3	SRC002	5001 - 6000	Raw residuals
-3	SRC002	5001 - 6000	Correlation count
4	REC001	1 - 256	Raw residuals
-4	REC001	1 - 256	Correlation count
5	REC002	1001 - 1256	Raw residuals
-5	REC002	1001 - 1256	Correlation count

Each block (either raw residuals or correlation count) is formatted as follows. The checksum is an exclusive - or checksum of all the data (words 1 to n-1) with the block.

<u>WORD</u>		
1	Block number
2 - 4	Source or receiver line name
5	First source or receiver point this record
6	Last source or receiver point this record
7		
.	Raw residuals or correlation count
.	for each source or receiver point
n - 1		
n	Checksum

APPENDIX "F"

WEEKLY OPERATIONS SUMMARY REPORTS

GEO SYSTEMS PTY. LTD.
173 PLANET STREET,
CARLISLE, W.A. 6101

Party No. 201
Party Head: H. ALTHORN

Address & Phone No. AMBASSADOR, 100/110, 322/2
Phone No. 443 3222

Client: HARTGEN
Client Rep: CLAU'S KUGBALL
Location: SALE VIC.
Week Ending: 6/1/73

WEEKLY OPERATIONS SUMMARY

DAY/DATE	WEEK							TOTALS	TITLE	LIST ALL HOURLY PERSONNEL AND HOURS WORKED	MONTHLY SALARIED PERSONNEL						
	M	T	W	TH	F	S	S				M	T	W	TH	F	S	S
RECORD. HRS.	4.0	9.0	9.0	8.0	7.5	80.5		VIB. OPS	B. ORRCH	-	11 1/2	10 1/2	10 1/2	11 1/2	15	P.M.	H. ALTHORN
TRAVEL HRS.	1.0	1.0	1.0	1.0	1.0	5		S. FINDR	10	8	11 1/2	10 1/2	10 1/2	12 1/2	"	M. SHADLUND	
OTHER PD. HRS.	5.0	1.5	0	1.0	0.5	8		L. DEAN	-	11 1/2	10 1/2	10 1/2	10 1/2	55	"	T. WELSH	
TOTAL PD. HRS.	10.0	11.5	1.0	1.0	11.5	53		D. WILKINSON	10	8	11 1/2	10 1/2	10 1/2	73	OPERATOR	C. RYAN	
PROFILES								B. MURPHY	13	10 1/2	10 1/2	10 1/2	11 1/2	82	"	W. L. HUNT	
PROD. 1st VIB. No								B. MURPHY LTD	12	10 1/2	10 1/2	10 1/2	12	75.5	TECHNICIAN	J. S.	
ACTUAL								K. ADOLAN	-	9 1/2	8 1/2	8 1/2	8 1/2	44.25	WIRE DRILL	W. SHADLUND	
No. AT.U. OPER.								A. WELSH	-	10	11	8	10	10 1/2	49.5	W	P. ALPHONSO
No. VIB. OPER.								R. GARRA	-	10	11	8	10	10 1/2	44.5	W	T. ALTHORN
F.L.D. PROC. HRS.								A. STEWART	-	10	10 1/2	10	10 1/2	51	SURVEY	W. T. ALTHORN	
WEATHER															PROC. SORC	W. T. ALTHORN	

OPERATIONAL PARAMETERS AND EQUIPMENT

AV. ROAD COND.	AV. FLD. COND.	AV. REC. QUAL.	VIB. TYPE	VIB. ELECT. (PELTON)	V.P. INTERVAL	SMSV/P.	SPREAD CONFR.	COMMENTS, VISITORS, PARAMETERS, PERSONNEL, ETC.
GOOD	GOOD	GOOD	LES 3/1	10 Hz	30	6	25%	2. Start case. CO'S (PM) - Long and Vol. Survey.
								3. Test Begin V Test (7 m) - Production Sample - (4.5)
								5: Production with Buggies
								Visitors - Faint O'Sullivan (Geosystems)

LOST RECORDING TIME ANALYSIS

HOURS	REASON	PERSONNEL	TIME
1	Equipment Breakdown	B. ORRCH	1:00
1	Equipment Breakdown	M. SHADLUND	1:00
1	Equipment Breakdown	T. WELSH	1:00
1	Equipment Breakdown	C. RYAN	1:00
1	Equipment Breakdown	J. S.	1:00
1	Equipment Breakdown	P. ALPHONSO	1:00
1	Equipment Breakdown	T. ALTHORN	1:00
1	Equipment Breakdown	W. T. ALTHORN	1:00

COMPLETED BY: H. ALTHORN

FORM 0963

Address & Phone No.: AMBASSADOR HOTEL, SALE, 443 222
 Client Rep: CLAU S. KUWALL, Location: SALE, VIC

Geo Systems Pty. Ltd. Party No. 204
 Party Head: H. ATHORN

DAY/DATE	M	T	W	TH	F	S	S	S	S	TOTALS	TITLE	MONTHLY SALARIED PERSONNEL
RECORD. HRS.	3.5	7.75	7	9	9.25	7.4	8-3	52.2		WEEK (MTH)		NAME
TRAVEL HRS.	1.0	1.0	0.5	1.0	1.0	1.0	6.5					H. ATHORN
OTHER PD. HRS.	3.5	-	2.75	-	-	1.1	7.35					K. PERKMAN
TOTAL PD. HRS.	8.5	9.5	11.75	10	10.75	10	9.8	70.3				H. HUME
PROFILES	53	136	107.7	178	232	160	1063					P. KILPATRICK
PROD	1st VIB. No	162	321	344	893	301	1663					S. STEVENS
ACTUAL	1.68	4.2	4.82	5.37	7.02	4.92	30.34					G. PARRETT
No. A.T.U. OPER.	85	90	86	87	85	90	82	102				I. ALLEGRI
No. VIB. OPER.	3	3	3	3	3	3	3					T. WILSON
F.L.D. PROC. HRS.	9.5	9.5	9.5	10	10.5	9.5	10	68.5				C. JAYSON
WEATHER	clear	fine	sun	clear	fine	fine	fine					P. JAMESON

OPERATIONAL PARAMETERS AND EQUIPMENT		SYSTEM No. 318	
AV. ROAD COND.	Geo	GEO. INTERVAL	10
AV. F.L.D. COND.	Mid	GEO. GRP.	6
AV. REC. QUAL.	Good	TOTAL GEO. STRINGS	1602
VIB. TYPE	4.5 311	GEO. MFG./TYP.	MKL21A
VIB. ELECT. (PELTON)		AT.U. TYPE	GSC No 2
V.P. INTERVAL	30	GEO. INT. RES.	10 Hz
SWPS/V.P.	6	GEO. BASE	SRK
SPREAD CONF	20.0	TOTAL CABLES	168
		SWEEP TIME	8 SEC.
		LISTEN TIME	4 SEC.
		SAMPLE RATE	2 MS

COMMENTS, VISITORS, PARAMETERS, PERSONNEL, ETC.

HOURS	LOST RECORDING TIME ANALYSIS	TITLE	NAME	M	T	W	TH	F	S	S	S	Total	TITLE
M 1.5	VIB. ROAD 100% Pass.	BOY TRUCK	B. CARTER	11	10	10	10	10	10	10	10	78.5	VIB. SER.
T 1.5	VIB. Road line Position	D. ROSSON	D. ROSSON	10	10	10	10	10	10	10	10	79.25	PERSON.
W 0	VIB. Road line Position	G. WILKINS	G. WILKINS	11	10	10	10	10	10	10	10	72	UTILITY
TH 1.0	VIB. Road line Position	G. WILKINS	G. WILKINS	11	10	10	10	10	10	10	10	72.5	UTILITY
F 0	VIB. Road line Position	G. WILKINS	G. WILKINS	11	10	10	10	10	10	10	10	71	UTILITY
S 0.5	VIB. Road line Position	G. WILKINS	G. WILKINS	11	10	10	10	10	10	10	10	71	UTILITY
S 1.45	VIB. Road line Position	G. WILKINS	G. WILKINS	11	10	10	10	10	10	10	10	71	UTILITY

COMPLETED BY: H. ATHORN

WEEKLY OPERATIONS SUMMARY

GEO. SYSTEMS PTY. LTD. Party No.: 209
 177 LANSET STREET, CARLE Place, W.A. 6101
 Party Head: P. JAMESON
 Address & Phone No.: APO GASSARDOS HOTEL, SALE
 Client: HARTOGEN
 KUBALL location: WILKORRA
 Week Ending: 27.10.1985

DAY/DATE	WEEK							TOTALS	TITLE	LIST ALL HOURLY PERSONNEL AND HOURS WORKED							MONTHLY SALARIED PERSONNEL						
	M 21	T 22	W 23	TH 24	F 25	S 26	S 27			WEEK MONTH	M	T	W	TH	F	S	S	Total	TITLE	NAME			
RECORD. HRS.	10.75	4.5	8.5	8.0	6.1	7.0	8.5	53.25	VIB. OP'S	B. DABCH	10/26/12	10/27/12	10/28/12	10/29/12	10/30/12	10/31/12	79 1/2	P. M.	P. JAMESON				
TRAVEL HRS.	1.0	1.0	1.0	1.0	1.0	1.0	1.0	7.0	"	J. TING	10/26/12	10/27/12	10/28/12	10/29/12	10/30/12	10/31/12	79 1/2	PASSENGER	K. GERARD				
OTHER PD. HRS.	0.5	0.5	0.5	0.5	0.5	0.5	0.5	3.5	"	S. WATLEY	10/26/12	10/27/12	10/28/12	10/29/12	10/30/12	10/31/12	79 1/2	"	H. HUME				
TOTAL PD. HRS.	2.25	2.0	2.0	2.0	2.0	2.0	2.0	13.0	"	P. HARRIS	10/26/12	10/27/12	10/28/12	10/29/12	10/30/12	10/31/12	79 1/2	"	P. KATING				
PROFILES	237	101	206	149	183	100	655	1311	"	"								"	P. JAMESON				
PROD. 1st VIB. No	829	2083	1283	547	100	655	1179	1179	"	"								"	L. JAVANABA				
ACTUAL	7.50	3.0	6.12	4.5	5.52	7.02	34.7	117.97	"	"								"	G. GAITHERY				
No. A.T.U. OPER.	89	86	86	86	85	86	86	86	"	"								"	J. DEDICAT				
No. VIB. OPER.	3	3	3	3	3	3	3	3	"	"								"	T. MURPHY				
FLD. PROC. HRS.	4.75	4.5	4.5	4.5	4.5	4.5	4.5	24.75	"	"								"	P. JAMESON				
WEATHER	FINE	FINE	FINE	FINE	FINE	FINE	FINE	FINE	"	"								"	P. JAMESON				
OPERATIONAL PARAMETERS AND EQUIPMENT																							
AV. ROAD COND.	GOOD	GEO. INTERVAL	10	SYSTEM No.	318																		
AV. FLD. COND.	GOOD	GEO. GRP.	6	SYSTEM MFG.	GEK																		
AV. REC. QUAL.	GOOD	TOTAL GEO. STRINGS	1102	TAPE FORMAT	GEK 411																		
VIB. TYPE	GE. S11	GEO. MFG./TYP.	DUK 21A	A.T.U. TYPE	GEK N-2																		
VIB. ELECT. (PELTON)		GEO. FREQ.	10 HZ	NOTCH FILTER	OUT																		
V.P. INTERVAL	50	GEO. INT. RES.	1000 SL	TRACES/FILE	512																		
SWPS/V.P.	6	GEO. BASE	SPRING	SWEEP TIME	8 SEC.																		
SPREAD CONFR	2500-0	TOTAL CABLES	168	LISTEN TIME	4 SEC.																		
	2500			SAMPLE RATE	2 MS																		
COMMENTS, VISITORS, PARAMETERS, PERSONNEL, ETC.																							
VISITORS: T. BAY ARRIVED ON 25-01-'85.																							
LOST RECORDING TIME ANALYSIS																							
M 10	Recording jump picks and vibration problems																						
T 10	bad cables																						
W 10	technical boxes																						
TH 10	vibe packs - cables																						
F 10	vibe packs - cables																						
S 10	bad cables and changing cables																						
S 10	bad cables																						

COMPLETED BY: P. JAMESON

173 PLAZET STREET
 CARLISLE, W.A. 6101
 STEMS PTV. LTD.
 Party No. 201

Party Head: P. JAMIESON

Address & Phone No.: AMBASSADOR HOTEL, SALE
 Client: HARTOGEN

Client Rep: G. KUBALL
 Location: SALE, VIC
 Week Ending: 03/10/78

WEEKLY OPERATIONS SUMMARY

DAY/DATE	TOTALS							WEEK MONTH	TITLE	LIST ALL HOURLY PERSONNEL AND HOURS WORKED							MONTHLY SALARIED PERSONNEL						
	M	T	W	TH	F	S	S			M	T	W	TH	F	S	S	Total	TITLE	NAME				
RECORD-HRS	9.25	7.25	8.5	8.5	7.75	8.5	8.75	58.00	24.50	VIB-OP	B. DARGY	12	14	12	11/2	10	50.0	P.N	P. JAMIESON				
TRAVEL HRS	1.0	1.0	1.0	1.0	1.0	1.0	7.00	3.00	"	TINA	12	14	12	11/2	10	84.4	OPER VIB	R. PERMATH					
OTHER PD. HRS	0.75	0.5	0.5	0.5	0.5	0.5	6.25	8.00	"	S. WHALLEY	12	14	12	11/2	10	84.4	"	H. WILSON					
TOTAL PD. HRS	10.75	8.25	10	10	11	10	10.50	11.50	"	P. M. JAMES	12	14	12	11/2	10	84.4	"	P. RATHBONE					
PROFILES	241	180	200	208	166	232	201	1478	595	"	M. SMITH	12	15	11	12	12	134	IR. OPERATOR	S. TAYLOR				
PROD	1st VIB. No	1357	2065	1525	925	292	1741	1039	"	C. OMA	13	12	-	-	-	25	OPERATOR	L. JAYARAMA					
ACTUAL	7.23	5.37	6.0	6.33	5.01	7.02	6.00	43.02	18.07	"	P. MEGGITT	13	12	10	10	10	71.4	LAND TECH	G. CALVERT				
No. A.T.U. OPER.	86	85	85	85	85	86	86	"	"	"	"	"	"	"	"	"	"	"	I. MEGGITT				
No. VIB OPER.	3	3	3	3	3	3	3	"	"	"	"	"	"	"	"	"	"	"	T. HEDDLE				
FLD. PROC. HRS.	10.0	10.0	10.0	9.25	5.5	10.5	14.00	17.00	21.10	"	K. D. AID	10	10	10	10	10	71	"	K. D. AID				
WEATHER	FINE	FINE	W/M	RAINY	FINE	FINE	HOT	"	"	"	"	"	"	"	"	"	"	"	"				
OPERATIONAL PARAMETERS AND EQUIPMENT																							
AV. ROAD COND.	GOOD	GEO. INTERVAL	10	SYSTEM No.	215	FIELD-CLEAR	E. RATHBONE	10	10	10	10	10	10	10	10	71.4	PM	"					
AV. FLD. COND.	ROUGH	GEO. GRP.	6	SYSTEM MFG.	65C	"	"	"	"	"	"	"	"	"	"	"	"	"	"				
AV. REC. QUAL.	GOOD	TOTAL GEO. STRINGS	1102	TAPE FORMAT	600	GP1	A. TEREGO	12	12	12	12	12	12	12	12	73.4	PERMIT	"					
VIB. TYPE	LES 311	GEO. MFG. TYPE	MLK21A	A.T.U. TYPE	65C	No. 2	K. NOLAN	12	12	12	12	12	12	12	12	80	SURVEY	C. R. ILLI					
VIB. ELECT.	(PELTONI)	GEO. FREQ.	10 HZ	NOTCH FILTER	OUT	"	"	12	12	12	12	12	12	12	12	83.2	RECORD	C. R. ILLI					
V.P. INTERVAL	30	GEO. INT. RES.	1000 SL	TRACES/FILE	512	"	"	12	12	12	12	12	12	12	12	80.4	CABLE	C. R. ILLI					
SWPS/V.P.	6	GEO. BASE	512	SWEEP TIME	8	SEC.	B. CARTER	12	12	12	12	12	12	12	12	80.4	VIBRATOR	C. R. ILLI					
SPREAD CONFR.	2500-0	TOTAL CABLES	168	LISTEN TIME	4	SEC.	"	"	"	"	"	"	"	"	"	"	"	"	"				
	2500	SAMPLE RATE	2	MS	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"				
COMMENTS: VISITORS, PARAMETERS, PERSONNEL, ETC.																							
31/85 Jy Roy. D. Scaevon Lene } visitors																							
30/1/85 S. Scaevon - HARRISON Powers wire } visitors																							
UTILITY																							
K. TENKINS																							
O. BURB																							
V. CONLAN																							
M. JONES																							
C. HUGHES																							
T. M. COXWELL																							
P. DELIBALOS																							
L. DEAN																							
A. DAVIS																							
R. STRAW																							
A. TAPLEY																							
G. THOMPSON																							
C. RYAN																							
P. HEDDLE																							
I. CARTER																							
COMPLETED BY: G. HARRISON																							

LOST RECORDING TIME ANALYSIS

HOURS

T 0.75 0.5 Tuning up RADIO 10.25 BAD BOX

W 0.25 0.25 VIBE DOWN

TH 1.0 0.5 RADIO - 0.5 BAD CABLE

F

S 0.75 Simms Problem.

S 0.5 1.0 Simms Box

FORM 0763

DAY/DATE	WEEK							TOTALS	WEEK MONTH	TITLE	LIST ALL HOURLY PERSONNEL AND HOURS WORKED							MONTHLY SALARIED PERSON						
	M	T	W	TH	F	S	S				M	T	W	TH	F	S	S	Total	TITLE	NAME				
RECORD. HRS	6:75	7:75	7:00	9:05	7:25	7:5	8	51:75	132:5	VIB-OP	J. FINN	11 1/2	12	12 1/2	10 1/2	11 1/2	11 1/2	91 1/2	P.M	P. JAMIEBSON				
TRAVEL HRS	1:00	1:00	1:00	1:00	1:00	1:00	1:00	7:00	17	"	P. McINNES	11 3/4	12	12 1/2	11 1/2	11 1/2	82 1/2	A.P.M	S. BARRO					
OTHER PD. HRS	1:75	1:0	1:75	1:25	1:75	2:0	1:5	12:0	32	"	L. DEAN	11 3/4	12	12 1/2	11 1/2	11 1/2	78 1/2	LAB SERVER	S. PERMAN					
TOTAL PD. HRS	9:5	9:75	9:75	10:75	11:00	10:5	10:5	71:75	177	"	T. Mc CORBELL	11 3/4	12	12 1/2	11 1/2	11 1/2	85 1/2	TR. OBSERVER	S. JEVYAS					
PROFILES	2:02	2:21	2:57	1:25	1:48	2:18	2:34	18:91	50:15	"	B. DASCHE	-	-	-	-	-	11 1/2	VIB. TECH	P. KILPAT					
1st VIB. No	14:6:2	8:59	19:00	5:10	5:30	5:57	5:57	9:1		SURVEY	M. SMITH	11	10	11 1/2	11	10	11	75 1/4	"	R. GRIME				
ACTUAL	6:03	6:43	5:7	7:01	6:03	6:33	7:02	4:76	108:9	"	A. TAPLEY	11	11 1/2	11 1/2	10	10	10	76	SURVEYOR	R. LOSLIE				
No. A.T.U. OPER.	91	90	92	90	85	97	90			"	G. WILLIAMS	11	10	11 1/2	11	10	10 1/2	74 3/4	"	T. NEUM				
No. VIB. OPER.	3	3	3	3	3	3	3			"	B. MURPHY	11 1/2	13 1/2	12	12 1/2	12	12	94	PROCESSOR	R. HILDAL				
F.L.D. PROC. HRS	11:75	11:75	11:25	11:75	11:50	11:75	11:75	91:5	190:88	"	P. JENSEN	-	-	-	-	-	-		SERVER	M. SEME				
WEATHER	FINE	FINE	FINE	FINE	FINE	FINE	VERY WINDY	FINE		"	H. WERTHEIM	10 1/2	10	10	9 1/2	10	10	69 1/2	SURVEYOR	R. MATH				

OPERATIONAL PARAMETERS AND EQUIPMENT

AV. ROAD COND.	GOOD	GEO. INTERVAL	10	SYSTEM No.	218
AV. FLD. COND.	ROUGH	GEO. GRP.	6	SYSTEM MFG.	GSC
AV. REC. QUAL.	GOOD	TOTAL GEO. STRINGS	1102	TAPE FORMAT	1600 RPI
VIB. TYPE	LS 311	GEO. MFG./TYP.	MKL 21A	A.T.U. TYPE	GSC N° 2
VIB. ELECT. (PELTON)		GEO. INT. RES.	1000 SL	NOTCH FILTER	OUT
V.P. INTERVAL	30	GEO. BASE	SPIKE	SWEEP TIME	8 SEC.
SPRS/V.P.	6	TOTAL CABLES	168	LISTEN TIME	4 SEC.
SPREAD CONFR.	2560-0			SAMPLE RATE	2 MS
	2560				

COMMENTS, VISITORS, PARAMETERS, PERSONNEL, ETC.

PERSONNEL	HOURS	TITLE	PERSONNEL	HOURS	TITLE
A. DAVIS	11 5/12	UTILITY	F. CARSTER	11 3/4	VIB. SER.
C. RYAN	11 1/2	UTILITY	D. ROBINSON	11 3/4	VIB. SER.
P. DELAVALLOS	10 1/2	UTILITY	F. CARSTER	11 3/4	VIB. SER.
P. STRAW	10 1/2	UTILITY			
E. THOMPSON	10 1/2	UTILITY			
F. KERRIGAN	10 1/2	UTILITY			
J. CARTER	10 1/2	UTILITY			
P. MEGGITT	10 1/2	UTILITY			
D. BUBB	10 1/2	UTILITY			
M. JONES	11 3/4	UTILITY			
S. WHALLEY	10 1/2	UTILITY			
Y. CONLAN	10 1/2	UTILITY			

LOST RECORDING TIME ANALYSIS

HOURS	D/T	REASON	COMPLETED BY:
11	D/T	Rad Cable 1:0	
12	D/T	Computer Problem .5 Bad Cable .75	
13	D/T	Line Problem .75 Vibe .5	
14	D/T		
15	D/T		
16	D/T	Bad Terminal .25	
17	D/T	Bad Terminals and cables	

172 PLANET STREET,
CARLSB. W.A. 8101

Party No. 204
Party Head: P JAMIESON

Address & Phone No. AMGLASS ADOOR HOTEL, SAHLE

Client: HARTOGREN, Week Ending 24/2/85
Worked: C. KUBALL, Location: VICTORIA

WEEKLY OPERATIONS SUMMARY

DAY/DATE	WEEK							TOTALS	TITLE	LIST ALL HOURLY PERSONNEL AND HOURS WORKED							MONTHLY SALARIED PERSONNEL			
	M	T	W	TH	F	S	S			M	T	W	TH	F	S	S		Totd	TITLE	NAME
RECORD. HRS.	7.25	9.25	7.09	1.5				25.0	VIB-OP	T. FINN	12 1/2	12 1/2	13 1/2	11 1/2	9	9 1/2	10 1/2	78 1/2	EM	P. JAMIESON
TRAVEL HRS.	1.0	1.0	.5	.5				3.0		P. FINN	-	-	-	-	-	-	-	-	ACT	S. BARBOUR
OTHER PD. HRS.	4.50	1.50	1.75	1.0				9.25		L. DEAN	12 1/2	11 1/2	13 1/2	11 1/2	9	9 1/2	7	69	OBSERVER	E. B. PESHANN
TOTAL PD. HRS.	10.75	11.75	9.25	4.0				37.75		T. MCCORKELL	12 1/2	11 1/2	13 1/2	11 1/2	9	10 1/2	82	VIB. MECH	F. P. KILPATRICK	
PROFILES	1519	241	197	37				677		B. DARGH	12 1/2	12 1/2	13 1/2	11 1/2	9	9 1/2	78 1/2		VSA	R. GRAYES
PROD. ACTUAL	6.12	7.23	6.0	1.14				20.49	SURVEY	M. SMITH	11	10	10	13	11	10	9 1/2	73 1/2		R. LOSIER
NO. AT.U. OPER.	90	93	93	94						A. TABLEY	10	10	10 1/2	10 1/2	8	10	8	67 1/2	PROLESSOR	F. B. HUKISS
NO. VIB. OPER.	3	3	3	3						G. WILKINSON	11	10	10	13	11	10	8 1/2	73 1/2	OBSERVER	E/B. M. SEHLEN
FLD. PROC. HRS.	10.75	11.5	10.5	12.0				44.75		E. MURPHY	10 1/2	12 1/2	-	10	9	11	9 1/2	67 1/2	SURVEYOR	F. B. MATTHEW
WEATHER	FINE	FINE	FINE	FINE															VIB. TECH	F. G. JONES
OPERATIONAL PARAMETERS AND EQUIPMENT																				
AV. ROAD COND.	GOOD	GEO. INTERVAL	10	SYSTEM NO.	312				CAR-REP	A. WERTHEIM	10	10	10 1/2	10	9	11 1/2	3 1/2	62 1/2		J. PIERCE
AV. FLD. COND.	ROUGH	GEO/GRP.	6	SYSTEM MFG.	GSC					R. BLACK	10	10	10	13 1/2	8	9 1/2	3 1/2	60 1/2	LIST NO. OF ALL EQUIP. ON PARTY	
AV. REC. QUAL.	GOOD	TOTAL GEO. STRINGS	102	TAPE FORMAT	1600 BPL				FIELDER	L. LAINE	10	10	10	10	10	9 1/2	2	6 1/2	PERMIT	
VIB. TYPE	LES 311	GEO. MFG./TYP.	MKL 21A	AT.U. TYPE	CSC N° 2				LINE-BOSS	M. LUKAS	10 1/2	12	11	9	9	9	3 1/2	6 1/2	SURVEY	G.R. 172
VIB. ELECT. (PELTONI)	GEO. FREQ.	10 HZ	NOTCH FILTER	OUT															RECORD.	G.R. 932
V.P. INTERVAL	30	GEO. INT. RES.	1000SL	TRACES/FILE	512														CABLE	G.R. 165
SWPS/V.P.	6	GEO. BASE	5 P/K/E	SWEEP TIME	9	SEC.													VIBRATOR	Y. 293
SPREAD CONFR.	25600	TOTAL CABLES	168	LISTEN TIME	4	SEC.														Y. 291
	2560			SAMPLE RATE	2	MS														Y. 292
COMMENTS, VISITORS, PARAMETERS, PERSONNEL, ETC.																				
END OF RECORD ED 94																				
TOTAL Km 272.58																				
TOTAL CHARGABLE HRS 498.5																				
21 FEB - 85																				
LOST RECORDING TIME ANALYSIS																				
HOURS																				
10M																				
11T																				
12W	Instrument Problem																			
13TH																				
14F																				
15S																				

FORM C983

APPENDIX "G"

EQUIPMENT DOWNTIME AND LOST RECORDING
TIME ANALYSIS (PRODUCTION PERIOD ONLY)

2	January	:	1.00	hours vibrator down
4	"	:	7.00	tractors not working
7	"	:	1.50	hours vibrator problems
8	"	:	1.50	" line problems
10	"	:	1.00	" vibe "
12	"	:	0.50	" " "
13	"	:	1.45	" instrument problems
14	"	:	0.50	" bad terminals
16	"	:	1.25	" tape drive problems
18	"	:	2.50	" vibe line "
19	"	:	0.50	" radio-cable "
21	"	:	1.00	" recorder "
22	"	:	0.50	" bad cables
23	"	:	1.00	" bad terminal-boxes
24	"	:	1.00	" vibe problems
25	"	:	1.75	" vibe problems, line problems
26	"	:	2.25	" bad cables
27	"	:	0.75	" " "
29	"	:	0.75	" bad boxes
30	"	:	0.25	" vibe down
31	"	:	1.00	" radio problem
2	February	:	0.75	" sims problem
3	"	:	0.25	" bad box
4	"	:	1.25	" vibe stuck
10	"	:	1.00	" sim cable problems
11	"	:	1.00	" " " "
12	"	:	1.25	" computer problems
13	"	:	1.25	" line problems
16	"	:	0.25	" bad terminals
17	"	:	0.25	" bad terminals
20	"	:	2.75	" instrument problems

PLATE "A"

AREA LOCATION

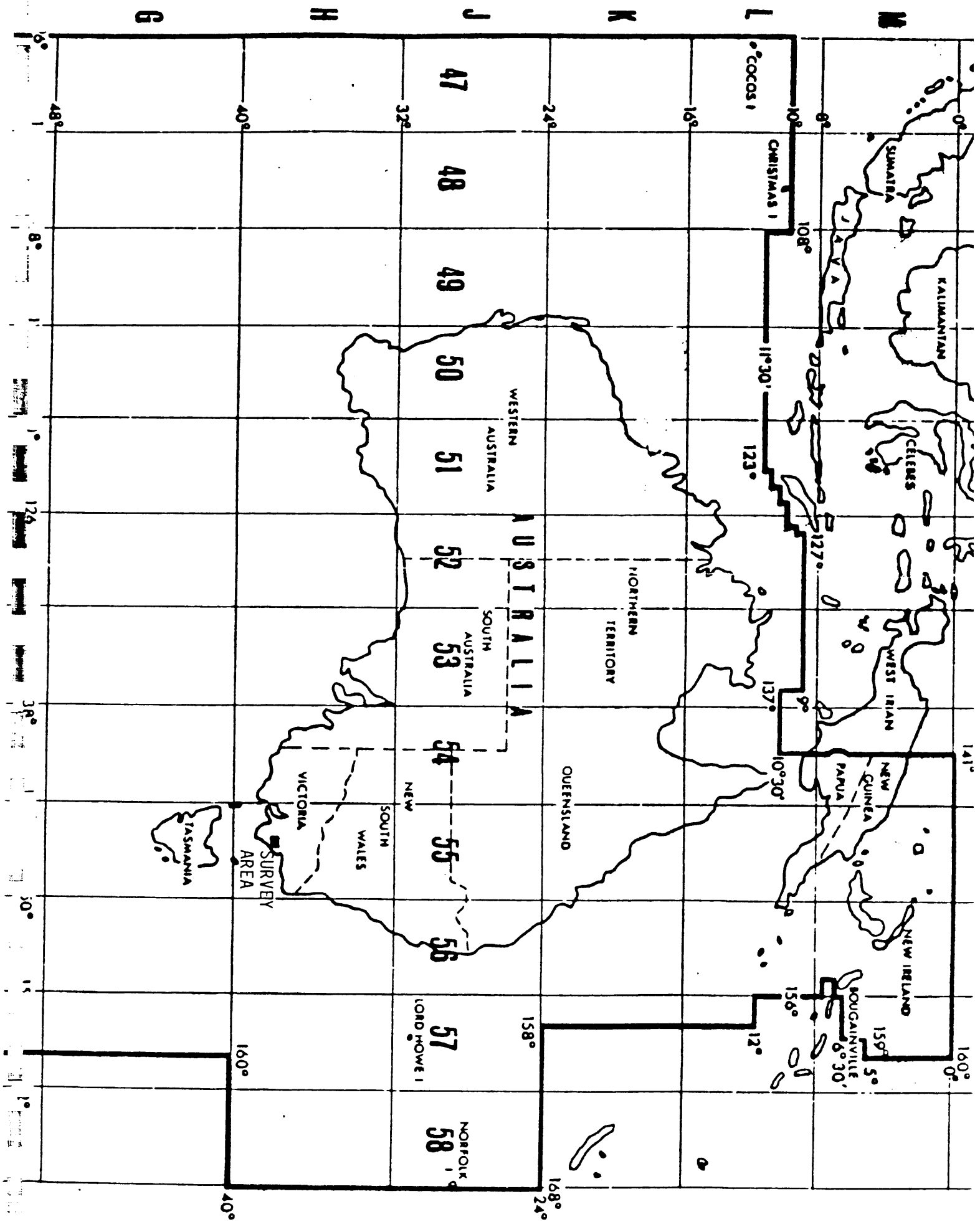


PLATE "B"

SOURCE ARRAY

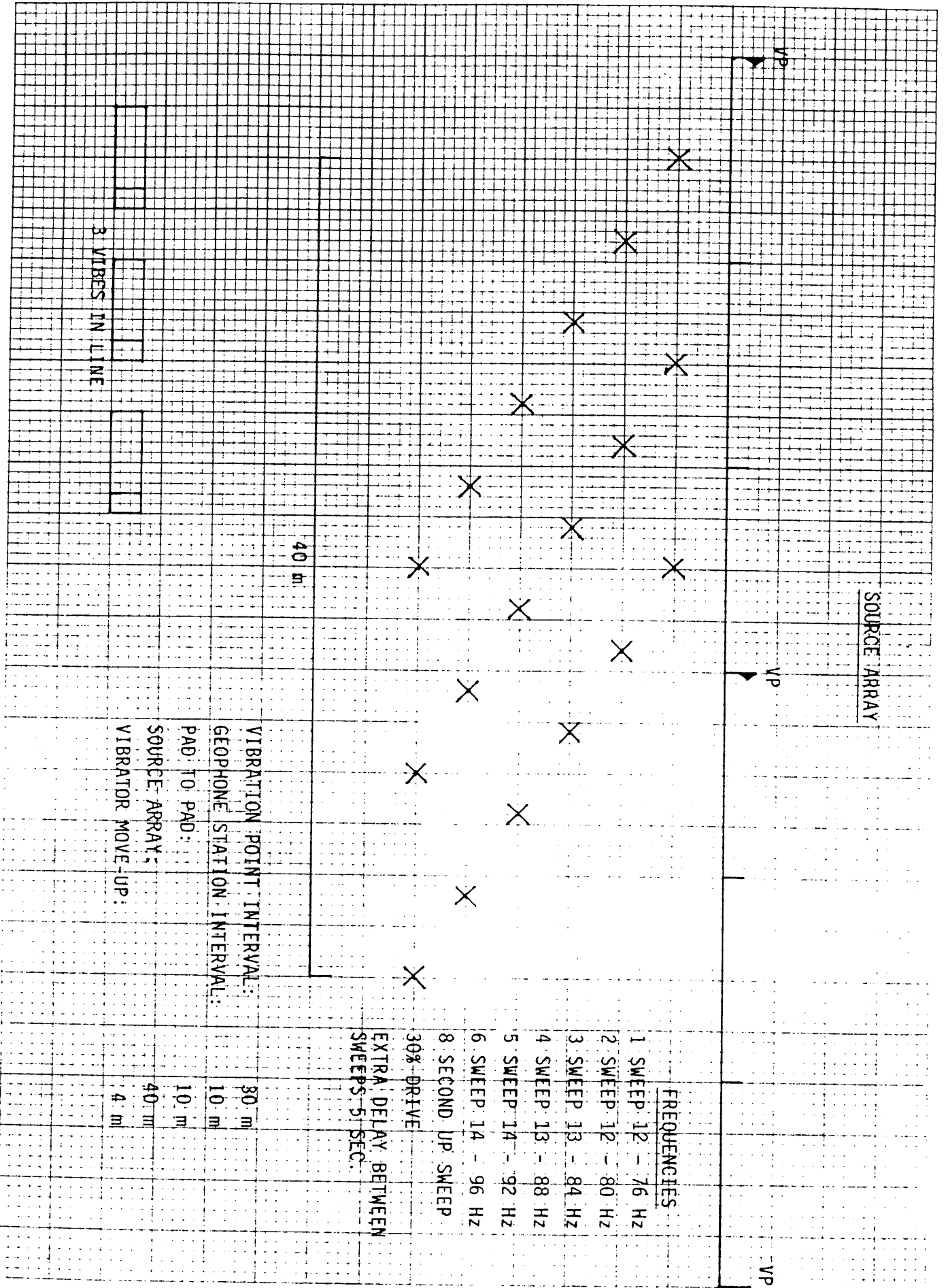
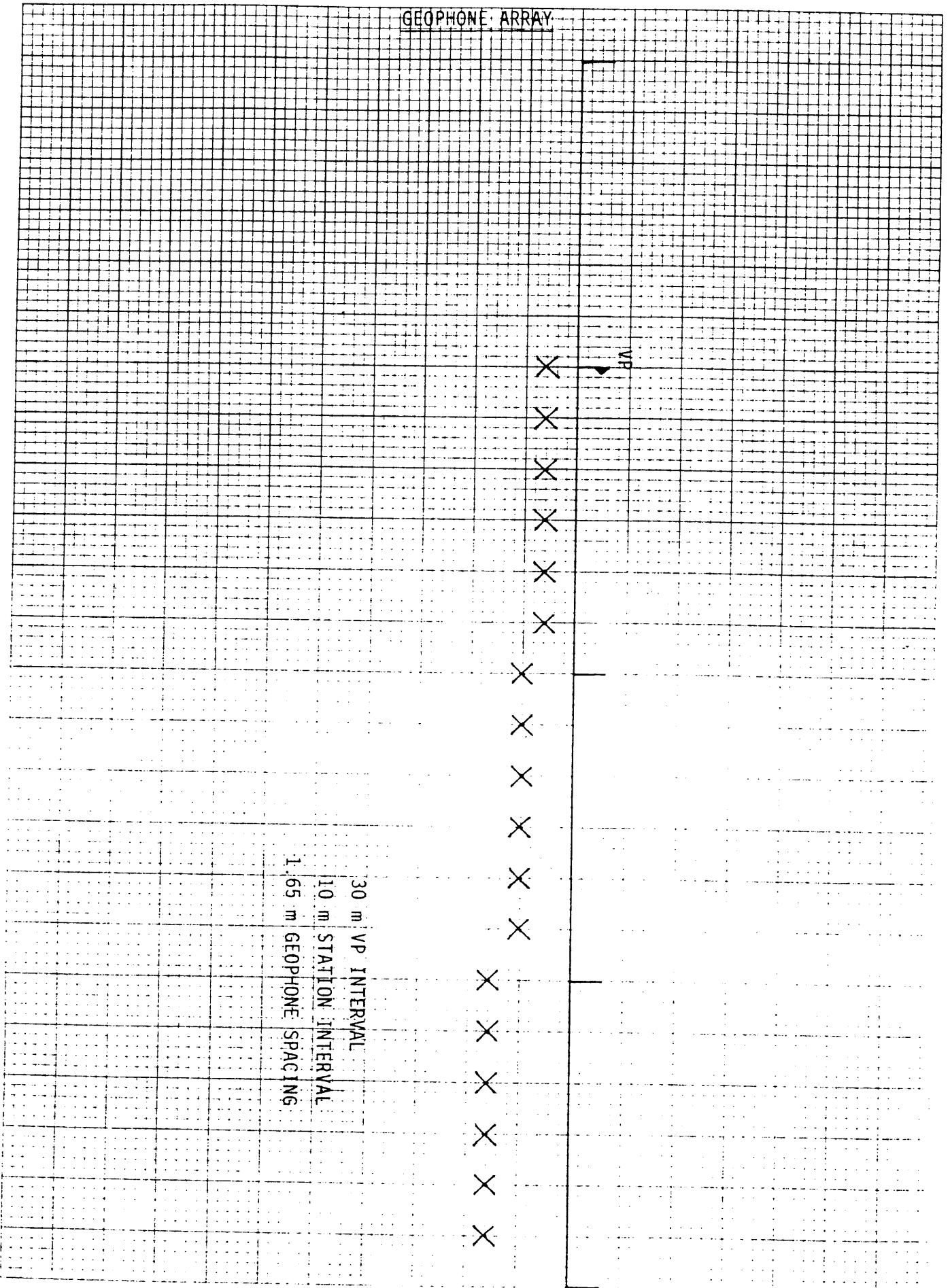


PLATE "C"

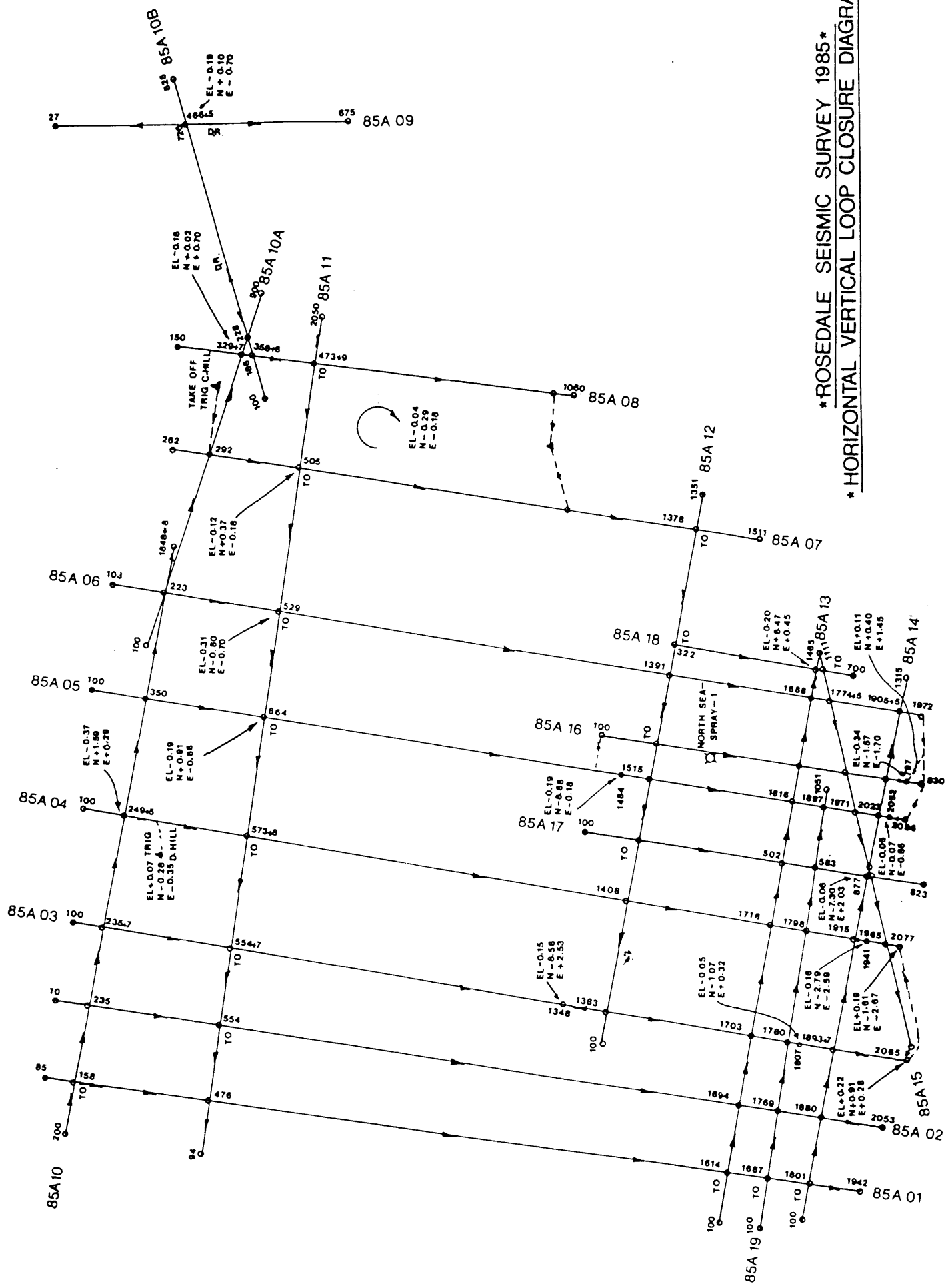
GEOPHONE ARRAY

GEOPHONE ARRAY



ENCLOSURE "A"

HORIZONTAL - VERTICAL LOOP CLOSURE MAP



ROSEDALE SEISMIC SURVEY 1985
 HORIZONTAL VERTICAL LOOP CLOSURE DIAGRAM

APPENDIX 2



DATA PROCESSING REPORT
GIPPSLAND BASIN
ROSEDALE SEISMIC SURVEY
PEP 109

FOR

HARTOGEN ENERGY LTD
15 YOUNG STREET
SYDNEY NSW 2000

BY

GEOPHYSICAL SERVICE INC.
6-10 TALAVERA ROAD
NORTH RYDE NSW 2113

SEPTEMBER 1985



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SECTION 1

INTRODUCTION

The Rosedale seismic reflection survey on permit PEP 109 in Victoria was recorded by GEOPHYSICAL SYSTEMS party No. 204. traverse were recorded through january and february, 1985.

Data were recorded split spread using a 512 trace cable, a 10 metre group interval, a near offset of 5 metres, and a far offset of 2565 metres. Vibroseis was used as the seismic source which resulted in a high frequency content. Data were recorded and processed for 86 fold CDP coverage.

Datum statics were computed using the times recorded on an uphole survey and is described in Section 2 of this report. Digital processing was performed by Geophysical Service Inc. in the Sydney Processing Centre using an IBM 3033 computer system. Production processing began in March 1985 and was completed by June, 1985. Details of collection and processing parameters, as well as purchase tapes are listed in the appendices of this report.



SECTION 2

DATUM STATICS

2.1 Collection and Computation Methods

Statics were computed from an uphole survey, using a two layer model with a constant replacement velocity of 1900 m/sec. The weathering layer produced a range of velocities from 500-1100 m/sec., with most lying in the 750-850 range, the sub-weathering produced a range of velocities between 1600-2300 m/sec., the average being approximately 1800 m/sec.

Shot and receiver statics were generally computed using weathering thicknesses and velocities linearly interpolated between upholes. However where discontinuities occurred in the weathering (due to Basalt flows) control uphole information was extrapolated from either direction to points close to the Basalt boundary with interpolation being carried out over the boundary.

This method assumes that all shots were located at the base of, or below, the weathered layer. This assumption was in general correct as evidenced from the implied uphole weathering velocity for most shots. There were however, some instances where the implied uphole velocity indicated that the shots had not penetrated through the weathering layer. At these locations, the field datum static anomalies were considered to be within the range of residual static corrections, and additional static computations were not performed prior to residual statics. This is verified by the actual residual statics, which were within the range of +5 to -5 milliseconds for both shots and receivers. The datum plane used for computations was mean sea level.



SECTION 3

PROCESSING

3.1 Experimental Processing

Experimental processing was performed on line GH85-7 as described below.

A)

1. TAR test: VP 647 and 677
No tar was used in the processing.

2. Velocity Filter test: VP 647
Velocity cuts of (6,-3) (8,-4) (10,-5) were tested
(8,-4) used for processing.

3. Scaling before stack: VP 341-741
Tested 500 msec. 1000 msec. 500 msec.(DGCS) 1000 msec.(DGCS)
500 msec. (DGCS) used.

4. Post stack deconvolution: VP 341-741
tested 16 msec. gap 100 msec. operator
20 msec. gap 100 msec. operator
No post stack deconvolution used.



5. Post stack Filter test: VP 341-741

Filter Analyses were performed on raw stack data. The frequencies used were:

0 - 250 Hz	15 - 60 Hz	20 - 70 Hz	25 - 70 Hz
10 - 60 Hz	15 - 70 Hz	20 - 80 Hz	25 - 80 Hz
10 - 70 Hz	15 - 80 Hz	20 - 90 Hz	25 - 90 Hz
10 - 80 Hz	15 - 90 Hz	20 - 100 Hz	25 - 100 Hz

Filter used for processing.

15-80 from 0-700 msec. 15-70 from 900-2500 msec.

linear interpolation of filters between 700 & 900 msec.

6. Post stack Scaling comparison: VP 341-741

Tested 500 msec. 1000msec. 500 msec. (DGCS) 1000 msec. (DGCS)

No post stack scaling used.

B)

Additional tests were run on line GH85-16 over VP 820-460 to confirm spread geometry. This consisted of:

1. Gathering the data into 3 CDP organized data sets, each data set reflecting a different spread configuration.
i.e. shot at 2535 metres from leading receiver group
shot at 2545 metres from leading receiver group
shot at 2555 metres from leading receiver group
(symetric spread)



2. Using the residual static program HSTATC, an estimate of residual shot and receiver statics were computed for the three data sets and these profiles displayed.

When the spread configuration was symmetric the residual shot static at the start of the line was considerably more positive than the respective residual receiver static, as the shot was moved towards the leading group, this gap closed. The configuration was assumed to be correct when this gap minimised. The spread geometry used for the Rosedale survey put the shot location at 2545 metres from the leading group.



3.2 Production Processing Sequence

The following sequence was used to process the data:

- * Datum static computation
- * Demultiplexing
- * Resample and Conversion to minimum phase
- * Pre-deconvolution ramp
- * Velocity filter
- * Designature
- * CDP gather and 3:1 CDP decimation
- * Time Variant Scaling
- * Velpac Velocity Analysis at 3km intervals
- * Brute stack
- * Residual static computation
- * Velpac Velocity Analysis at 1km intervals
- * Application of NMO, residual and datum
statics
- * 86-fold CDP stack
- * Filtering
- * Scaling
- * Film display
- * Migration of unfiltered stack
- * Filtering
- * Scaling
- * Film display

In addition to the film displays indicated above, the following sections were displayed on electrostatic paper:

- * Brute stack

A flow diagram of the above sequence is shown in Plate 1.



SECTION 4

CONCLUSIONS AND RECOMMENDATIONS

4.1 Data Collection.

The quality of data was in general good, with major problem being documentation regards the positioning of the shot with respect to the cable.

Experimentation to confirm location of shot is detailed in section 3.1 B above.

4.2 Datum Statics

In general there was no problems encountered with the datum statics.



4.3 Processing

Data quality was very good for the majority of the prospect. The exception was a small area in the north west of the survey. Incorrect documentation of the spread layout(already referred to above) proved to be a significant delay factor.

Although datum statics were adequate for most of the survey, residual statics resolved some significant static breaks, and should remain as a standard part of the processing sequence.

In poor S/N areas, a cost effective method of an improving S/N in the in the final stack may be achieved by using a decimation rate that is NOT an integer multiple of the shot moveup rate. Using such a rate of decimation allows residual statics to be estimated for every trace collected. All other final parameters can also be determined on the decimated data.

All traces can then be included in the final stack. Post stack migration enhanced the data quality, and should be part of the standard processing sequence for future processing of data from this area.

Respectfully submitted:
GEOPHYSICAL SERVICE INC.

Brian Helgareiff FOR ED BOYLAN

(Processing Party Chief)

GSI

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ROSEDALE



APPENDIX A

LIST OF LINES PROCESSED

LINE	SP RANGE	KMS	RECORDS
GH85-1	1942 - 85	18.60	620
GH85-2	10 - 2050	20.43	682
GH85-3	2065 - 100	19.64	657
GH85-4	100 - 2077	19.77	660
GH85-5	2083 - 100	19.83	663
GH85-6	106 - 1972	18.66	623
GH85-7	260 - 1511	12.51	418
GH85-8	162 - 1059	8.97	300
GH85-9	27 - 675	6.48	217
GH85-10	200 - 1847	16.47	550
GH85-10A	100 - 898	7.98	267
GH85-10B	100 - 823	7.23	242
GH85-11	2054 - 94	19.56	653
GH85-12	100 - 1351	12.51	418
GH85-13	1465 - 100	13.65	456
GH85-14	103 - 1315	12.12	405
GH85-15	100 - 1111	10.11	338
GH85-16	829 - 100	7.29	244
GH85-17	823 - 100	7.23	242
GH85-18	700 - 322	3.78	127
GH85-19	100 - 1051	9.51	318
TOTAL	21 LINES	272.33	9100

GSI

A-1

ROSEDALE



APPENDIX B

FIELD PARAMETERS

RECORDED BY	GEOPHYSICAL SYSTEMS
PARTY NUMBER	GSC NO 204
DATE	FEBUARY 1985
INSTRUMENTS	1024 CHANNEL - GEOCOR IV
GEOPHONE TYPE	MARK L21A 10 HZ
SAMPLE RATE	2 MSEC.
SOURCE	
VIBROSEIS	
SWEEPS	6 LINEAR UPSWEEPS
SWEEP LENGTH	8 SECONDS
SWEEP FREQUENCY	12 - 76 HZ
	12 - 80 HZ
	13 - 84 HZ
	13 - 88 HZ
	14 - 92 HZ
	14 - 96 HZ

GEOMETRY

NUMBER OF GROUPS	512
SPLIT SPREAD	2545 - 5 - 15 - 2565 metres
VP INTERVAL	30 metres
GROUP INTERVAL	10 metres
FOLD	86
PROGRESSION	TRACE 1 LEADING

GSI

B-1

ROSEDALE



APPENDIX C

PRODUCTION PARAMETERS

Typical processing parameters used are listed below and detailed parameters are appended to each final display section.

All data were processed at a 4msec sample rate and 2.5 seconds record time, but were displayed only to 2 seconds.

Datum was Mean Sea Level.

The surface referenced velocity functions used to stack the data were annotated on the header of each section.

C.1 Field Tape Translation.

All data was translated to an internal GSI format prior to processing.

C.2 RESAMPLE and CONVERSION TO MINIMUM PHASE

Data were resampled from 2 msec. to 4 msec. and converted from zero to minimum phase to comply with deconvolution assumptions.

C.3 PRE-DECONVOLUTION RAMP

	Time	Offset	Time	Offset	Time	Offset	Time	Offset
	msec.	metres	msec.	metres	msec.	metres	msec.	metres
Start times :	0	150	225	300	510	800	1640	2560
End times :	50	150	275	300	560	800	1690	2560

GSI

C-1

ROSEDALE



C.4 VELOCITY FILTERING

The velocity filter cuts were +8msec/trace and -4msec/trace which at a 10 metre group interval represents velocities of 2500 metres/sec and 7500 metres/sec respectively. The maximum frequency was 125 Hz. Version 5 velocity filter with normal cosine ramps was used.

C.5 DESIGNATURE

One wavelet was estimated for each record with a maximum frequency of 125 Hz. Version 5 Designature was used.

C.6 SCALING BEFORE STACK

Regular 500 msec. DGCS scaling gates were used for pre stack scaling.

this method uses 250 msec. of data either side of a data point to compute scalers for each sample point on the trace.

C.7 STACK RAMP

The production stack ramp was chosen from the single fold sections produced at the brute stack stage. The ramp is as follows:

Time (sec)	Offset (m)
0.000	150
0.400	600
1.100	1200
1.500	2560

This ramp was applied after relative statics and before mean statics and NMO.



C.8 RESIDUAL STATICS

Several space and time variant gates based on prominent reflectors were picked for each line. Three iterations were made. Gate lengths were varied according to the data on each line. A bandpass filter of 10-50Hz was used. The model smash was 11 depth points for all lines in this prospect.

C.9 VELOCITY ANALYSIS (VELPAC)

Relative statics plus residual statics were applied to the data before velocity analysis.

A 10-65 Hz bandpass filter was applied to the data.

C.10 MIGRATION

Dipcon migration was used for the entire prospect. Maximum allowable dip was 35 degrees, with velocity fields being conditioned from the stacking velocities using the Spacevels software. This conditioning whilst smoothing the stacking velocities maintained 100% of these velocities until 1.0 sec. from this point the values of the stacking velocities were gradually reduced until at 1.4 sec. they reached 90% of the original velocities. From 1.4 sec. to 2.5 sec. reduction to 90% was maintained.



C.11 BAND PASS FILTER

The following band pass bandpass filters were used in production.

Time (seconds)	Frequency (Hz)
0.000	10-85
2.500	10-85

C.12 DISPLAY PARAMETERS

Mode VA/WT

+-----+-----+					
: SECTION	TRACES/	CMS/	BIAS	MATERIAL	:
:	INCH	SEC			:
+-----+-----+					
: BRUTE STACK	12	7.5	0%	ELECTROSTATIC	:
:					:
: RESIDUAL STATICS	12	7.5	0%	ELECTROSTATIC	:
:				PAPER	:
:					:
: VELOCITY ANALYSIS	12	7.5	0%	ELECTROSTATIC	:
:				PAPER	:
:					:
: FINAL STACK	20	15	0%	FILM	:
:					:
:					:
: MIGRATION	20	15	0%	FILM	:
+-----+-----+					

All data were plotted normal polarity.



APPENDIX D

DESCRIPTION OF BASIC PROCESSES

D.1 PRE DECONVOLUTION RAMP

PDR is the process whereby first arrival unwanted noise at the front end of seismic records is removed. This is applied prior to deconvolution design.

D.2 VELOCITY FILTERING - VEF

Velocity filtering is a multichannel process that has been combined with designature into one executable load module. Multichannel filtering is a two dimensional frequency wave number operation used to discriminate against specified velocities on pre-stacked data.

Velocity filtering processing requires shot organised data that has a group interval representing adequate spatial sampling. Also, the receiver interval should be less than or equal to the shot interval to avoid aliasing.



The process transforms the data from the space-time domain (X-T) to the frequency-wave number domain (F-K) where the filter is applied. After filter application, the data is transformed back to the X-T domain for the application of further conventional processing.

The apparent horizontal velocity of the noise must be adequately separated from the primary signal for the process to be effective. Examples of noise alignment that can be removed are ground roll and air blast.

These types of noise have a slower apparent velocity than the primary signal or have a dip opposite to the primary. The user supplies a window of primary dip zones to keep; negative dip noise and positive dip noise outside of the keep zones are rejected. These keep and reject zones are usually designed from shot record displays and F-K analyses performed on these records.

Version 5 velocity filtering makes use of "cosine" cut-off ramps, as opposed to the linear ramps of the previous versions. The net effect of the cosine ramps is to reduce the "edge effects" which show as energy alignments parallel to the cut-off dips used in the process. The result is a cleaner record compared to the outputs from previous versions.

D.3 DESIGNATURE

Designature is a prestack deconvolution designed to collapse the effective source wavelet (or "signature") to a short, sharp zero phase wavelet and thus maximise resolution on the seismic traces. The effective source wavelet is the wavelet resulting from the convolution of the actual source wavelet with ghost effects, near surface short period reverberations and the recording instrument



response, although on land data, ghost effects are at a minimum. Designature does not take account of additive noise in its design, but assumes that noise is absent or negligible. Therefore it is important to attenuate both coherent and non-coherent additive noise prior to Desig in order to comply as closely as possible with this assumption. This emphasises the importance of the velocity filtering, editing and pre-deconvolution ramp that is done before Desig in the wavelet processing sequence.

One of the fundamental assumptions made in Desig is that the average amplitude spectrum of the record is identical to the average amplitude spectrum of the effective wavelet which is the result of the convolution of several other wavelets or effects.

The phase spectrum of the source wavelet is important since Desig does not measure it, but assumes it to be minimum phase. Most sources have phase spectra approximating minimum phase, excepting Vibroseis* which requires preliminary processing to both collapse the sweep and convert it to a minimum phase characteristic.

D.4 TIME VARIANT SCALING-TVS

Time Variant Scaling produces amplitude equalisation in a time variant manner down the seismic trace as well as from trace to trace. Scalers computed for each gate are applied at the gate centre, with linear interpolation between gate centres. Gate amplitudes are measured for a set of continuous gates on each trace and scalers are computed for each gate to make the average amplitude constant within each gate. This amplitude is 2×10 .

* Trademark of Continental Oil Co.



D.5 PRELIMINARY VELOCITY ANALYSIS - VELPAC

The Velpac velocity module was applied in the spot analysis mode using 11 adjacent depthpoints and 5 sets of moveout corrections. Basic steps of the programme for each analysis include:

- Application of normal moveout (NMO) corrections, corresponding to several different constant velocities or velocity functions, to a set of adjacent depthpoints, followed by CDP stacking.
- A time gated, power based search of the stacked traces to provide picks as functions of time, amplitude, and moveout (which is another expression of velocity).
- Display of selected depthpoint gather traces, stack traces, and power picks.

D.6 PRELIMINARY STACKS

Preliminary stacks with datum statics, single fold sections, and near trace gather sections were produced. Initial velocities were obtained from Velpac velocity analyses performed at 3 km intervals. These sections had several uses:

1. As a quality check on the processing.
2. To give an initial look at the data and identify potential problem areas.
3. To evaluate the velocity functions used.
4. To evaluate the datum statics.
5. To evaluate the prestack mute.
6. To enable selection of design gates for residual static computation.
7. To assist in horizon selection for velocity interpretation.



D.7 AUTOMATIC RESIDUAL STATIC COMPUTATIONS

The method is based upon cross-correlation functions which are used to measure the relative time shifts for each of the traces within a common depth point set. Each of the traces of a CDP set is correlated with a reference trace formed by stacking the other traces within the set.

The location of the peak value of the cross-correlation function gives an estimate of the time shift of the static shifted trace. The time shift measured by the cross-correlation is the sum of several effects, namely:

- i. Residual shot static.
- ii. Residual receiver static.
- iii. Residual normal moveout.
- iv. Noise.

The correlation functions are computed over gates which are chosen such that the signal to noise ratio is high and little or no residual moveout is present.

The time shifts obtained from the correlation functions for each trace are then placed in tables of common shot and receiver positions, and a statistical analysis carried out to determine an unique residual source correction for each shot and an unique residual correction for each receiver. This ensures that at all times statics which are applied to data are surface consistent.

Finally, the statics to be applied are synthesised from the estimates of the individual shot and receiver statics by averaging the values along common source and receiver traces.



The process is iterative and several rounds are applied to achieve upgraded estimates of the residual statics to apply - the input to successive iterations being the output from the preceding round. To enable a check of the results, as well as a listing of the computed static, a plot was made of the selected gates with the computed residual statics applied after the final iteration. This plot was also displayed on the final film sections.

D.8 VELOCITY ANALYSIS - VELSCAN

The VELSCAN module used 11 adjacent depth points at each location. The following is a brief description of the process.

VELSCAN generates events as functions of time, amplitude, moveout and dip. The event picking proceeds in the following manner:

- NMO, Static and Residual Static corrections corresponding to a series of velocity functions are applied to a set of depthpoint traces. For each velocity function the NMO corrected traces are stacked. The resulting traces consist of amplitudes as functions of time and moveout.
- Identical operations are applied to adjacent depth points, adding the dimension of space.
- Dip is applied and, for each value of dip, the traces are stacked across depth points. The result is a set of amplitudes as functions of time, moveout and dip.
- An event is located by searching for an amplitude extremum in the time, moveout and dip domains. An extremum may be either a maximum or minimum; i.e. both peaks and troughs are picked. The event attributes of time, amplitude, moveout and dip are assigned to the centre depth point.



- Prior to display, the events are subjected to various sorting and classification algorithms. The powerful picking of VELSCAN yields good results even in relatively poor data areas.

As an aid to interpretation, the VELSCAN module also generates and displays the central CDP without NMO or static corrections and with each of the user supplied reference velocity functions, the stack traces for all depth points used within the scattergram, and the reference velocity functions are plotted on the scattergram.

For this survey the velocity analyses had relative datum statics and residual statics applied prior to NMO corrections.

D.9 APPLICATION OF DATUM STATICS

The application of datum statics was performed in the following manner:-

Prior to application of normal moveout corrections a "mean" datum static was computed for each depth point and a "relative" datum static computed for each trace within that common depth point set. The relative static was simply the difference between the mean datum static and the individual trace datum statics. The relative datum statics thus computed were then applied, together with the residual statics, to the traces prior to the application of normal moveout corrections. A consequence of this method of datum static application is that velocity functions for normal moveout corrections are expressed relative to the surface and not relative to the datum plane.



D.10 NORMAL MOVEOUT CORRECTIONS

Normal moveout corrections are applied to remove increased reflection time on an event caused by spread geometry. The magnitude of the event correction is determined by the following equation:

$$T = \frac{(T_o^{**2} + X^{**2})^{**0.5} - T_o}{V^{**2}}$$

where

T = Normal Moveout.

T_o = Time of the event at zero offset.

X = Offset of a trace.

V = Root mean square velocity of the event.

D.11 COMMON DEPTH POINT STACK

The traces for each depth point are summed to give one output trace for each depth point. Prior to the mix, first break energy plus the early portion of the traces where NMO corrections have caused severe stretching, resulting in significant frequency changes can be suppressed. The result of this is that the stacking multiplicity varies as a function of record time resulting in improvement of the continuity of shallow events.

D.12 TIME VARIANT FILTERING - TVF

Filtering is applied in a time variant manner to take account of the higher frequency content of the shallow seismic signal and the lower frequency content at depth when rejecting unwanted frequencies or noise. By appropriate filter design, unwanted frequencies are attenuated or removed.



D.13 MIGRATION VELOCITY CONDITIONING - SPACEVELS

SPACEVELS is the velocity modelling process designed for 3D data transformed to a 2D application. The user inputs stacking velocity functions and unmigrated horizon times and coordinates. SPACEVELS then uses an inline inverse ray tracing technique to produce a migration model defined in terms of depths and interval velocities, with the interval velocities referenced to the midpoint of each layer.

The input stacking velocity functions must be spaced frequently enough to adequately define the spatial velocity variations. The horizons selected need to define two essential properties of the model. These are the horizons at which there are major changes in the slope of the stacking velocity versus time functions, and the regional geologic dips present in the survey.

From the depth / interval velocity model, SPACEVELS computes the required velocity function. In this case, the RMS velocity along a zero offset normal incidence raypath for each horizon is computed, this being the input velocity required by the F-K domain migration program.

D.14. DIPCON MIGRATION

Controlled Wavefront Migration (DIPCON) implements the event mapping accuracy of GSI's previous F-K domain migration, with the cosmetic advantages of finite difference migration. This feature has been accomplished by simulating the dispersive character of the finite difference operators in F-K migration.



The normal F-K technique, being a wide angle algorithm, has a tendency to produce wavefront artifacts reaching into the shallow parts of the section when migrating data with noise bursts. The DIPCON technique will suppress the spurious wavefronts by attenuating them with a dip dependent energy dispersion algorithm. (The dip limit can be specified by the user). However the shape of the diffraction curve is not dip dependent as in finite difference migration, which uses a dip dependent approximation to diffraction mapping, and is therefore less accurate for migrating steeper dips.

DIPCON migration also reduces the mixed appearance sometimes apparent on the deeper data after normal F-K migration, preserving a character closer to that of the input stacked section.

A further consideration is mapping accuracy in the presence of lateral velocity variation. Most finite difference programs in use today are implemented as time migration; that is ray bending caused by the lateral velocity gradient is not taken into account. Under these circumstances events will overmigrate to the position given by the image ray. On the other hand, GSI's F-K domain migration (both normal and DIPCON) implemented with psuedo depth conversion will remove velocity induced dips before migration, and position events more accurately.



APPENDIX E

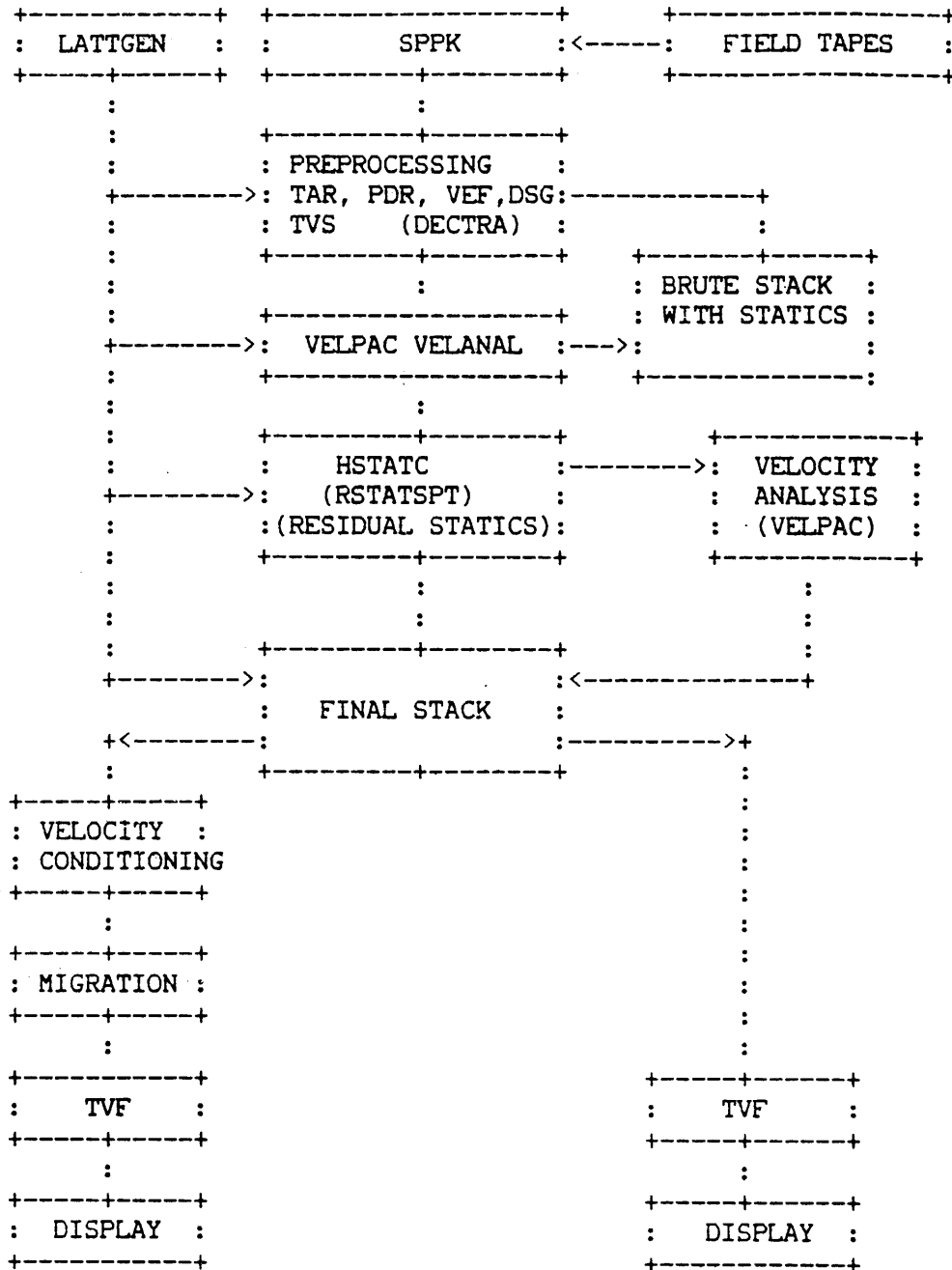
ROSEDALE HOLD TAPE (UNFILTERED DATA) LISTING

TAPE	CONTENTS
600652	CONSOLIDATED STACK DATA
600653	CONSOLIDATED MIGRATION DATA



PLATE 1

TIPEX PROCESSING FLOW CHART



GSI

ROSEDALE